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SHELLS SUBJECTED TO AXISYMMETRIC AND NEARLY  
AXISYMMETRIC STEP-PRESSURE LOADS USING SATANS-IIA,  
A MODIFIED VERSION OF SATANS-II

NAVAL POSTGRADUATE SCHOOL  
MONTEREY, CALIFORNIA

DECEMBER 1976

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# NAVAL POSTGRADUATE SCHOOL

## Monterey, California



# THESIS

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by

Michael D. Shutt

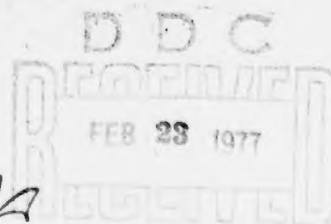
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Robert E. Ball

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PRESSURE LOADS USING SATANS-IIA, A MODIFIED VERSION OF  
SATANS-II

by

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Lieutenant  
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Submitted in partial fulfillment of the  
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## ABSTRACT

A digital computer program for the geometrically nonlinear analysis of totally arbitrarily loaded shells of revolution (SATANS-II) was modified to more accurately account for the conditions at the pole of the shell. This program was used to determine the buckling load of shallow spherical shells of various sizes when subjected to static axisymmetric, dynamic axisymmetric, and dynamic nearly axisymmetric step-pressure loads of infinite duration. A comparison was made between the new buckling results and previous results obtained without the new pole routine. The comparison revealed a significant change in the buckling pressures, due solely to the change in the pole routine. The new static axisymmetric, dynamic axisymmetric, and even the dynamic asymmetric critical buckling pressure loads appear to be fairly reliable results for perfect, shallow shells.

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# LIST OF SYMBOLS

$b$	= nondimensional inplane stiffness
$E$	= the modulus of elasticity of the shell
$H$	= the rise of the spherical cap at the pole
$h$	= the thickness of the shell
$m$	= the mass density of the shell
$M_s$	= the meridional bending moment per unit length
$n$	= the Fourier index
$P$	= a nondimensional applied load
$P_{CRIT}$	= the nondimensional critical pressure
$q_o$	= the classical buckling pressure of a complete sphere
$q^{(n)}$	= a column matrix containing the coefficients of the $n^{th}$ term in the series expansion of the applied load
$r$	= the normal distance from the axis of revolution to the surface of the cap
$r_o$	= the normal distance from the axis to the cap in the base plane; the maximum value of $r$
$R_s, R_\theta$	= the radii of curvature in the $s$ and $\theta$ directions, respectively
$s$	= the meridional distance along the surface of the shell
$t$	= the nondimensional time
$T$	= the time
$T_o$	= a reference time



$U, V, W$  = the displacements in the  $s$ ,  $\theta$  and  $J$  directions, respectively  
 $u, v, w$  = nondimensional series coefficients of  $U, V, W$   
 $\bar{V}$  = a nondimensional measure of the volume of the shell deformation  
 $\bar{V}_{MAX}$  = the peak in the time history of the parameter  $\bar{V}$   
 $w^{(n)}$  = the displacement in the  $J$  direction in the  $n^{th}$  harmonic  
 $\delta t$  = the nondimensional time increment  
           = distance between stations  
 $\epsilon^{(n)}$  = the nondimensional parameter governing the magnitude of the load applied in the asymmetric harmonics  
 $J$  = the coordinate normal to the surface of the shell  
 $\theta$  = the circumferential angle measured about the axis of revolution  
 $\lambda$  = a nondimensional geometric parameter used to describe the spherical cap  
 $\nu$  = Poisson's ratio  
 $\xi$  = the normal distance from the base plane to the middle surface of the undeformed cap

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## I. INTRODUCTION

In 1973 a digital computer study was presented by Ball and Burt [1] for the dynamic buckling load of clamped shallow spherical shells subjected to axisymmetric and nearly axisymmetric step-pressure loads. A static buckling analysis of the same spherical shells had been carried out in 1970 by Stilwell and Ball [2]. In these two studies the digital computer program SATANS-I [3] was used to calculate the critical buckling pressures for a large range of shell sizes. Other studies of the buckling of shallow shells have been conducted by Huang [4,5], by Stephens and Fulton [6], by Lock et al. [7], by Stricklin [8], and most recently by Akkas [9]. In Reference 1 the results from these other studies, except for those by Akkas, are compared with the results from SATANS-I for both static and dynamic buckling. In the axisymmetric static analysis the comparison with the results obtained by Huang [4] revealed that the SATANS-I results were higher than Huang's results for several shell sizes. In the dynamic, axisymmetric buckling analysis the SATANS-I results again either agreed closely with, or were somewhat higher than, the results by Huang [5], Stephens and Fulton [6], and Stricklin [8]. However, it was noted then that there was a general lack of consistent agreement among any of the sets of results. As a consequence, it appeared at that time that the axisymmetric buckling problem had not yet been totally resolved and that additional studies would be appropriate.

In the asymmetric dynamic buckling analysis of Reference 1 the few comparisons that could be made for the critical load also indicated that the SATANS-I results may be too

high. A comparison of the recent estimates for the asymmetric dynamic buckling load obtained by Akkas [9] with the SATANS-I results also reveals the SATANS-I results to be well above those of Akkas [9]. However, it should be noted that the results obtained by Akkas were from his attempt to obtain a lower bound on the critical asymmetric load. This bound on the buckling load is obtained without the execution of a complete transient response analysis on the asymmetric part of the response of the shell, as is done in SATANS-I. In Akkas' analysis (Problem 1) the transient nonlinear axisymmetric response is computed, and a determinant is examined for possible bifurcation into asymmetric motion at each time step. The minimum load at which the determinant becomes zero is defined as the lower bound of the critical load.

As a consequence of the generally high buckling loads predicted by SATANS-I, a re-examination of the static and dynamic buckling of the shallow spherical shell was made in an attempt to determine the possible cause, or causes, of the high buckling loads. In our search we discovered that a modification of the manner in which the pole conditions are numerically approximated significantly lowered the buckling loads to values that are now in good agreement with the other results. The new procedure for handling the pole condition is given in section III of this thesis. The new buckling results are given in section V.

In addition to the pole condition modifications and the new buckling results the author has also made another significant change to the SATANS family of codes. In particular, the SATANS-II program for the geometrically nonlinear analysis of totally arbitrarily loaded shells of revolution, developed by Ryan [10] in 1972 to handle more complex and larger problems, was modified to make the computer memory requirement a variable quantity. This

quantity is specified by the user to fit the particular problem being run. It eliminates the large core requirement of SATANS-II for small problems and allows for much larger problems to be solved than could be solved by SATANS-II. The new program with the pole condition and memory modifications will hereafter be called SATANS-IIA. It is described in section II.



## II. DESCRIPTION OF SATANS-IIA

SATANS-II was developed by Ryan [10] from SATANS-I and incorporated the full trigonometric expansion of the applied load and solution vector, and introduced the handling of imperfections into the code. These modifications allow the analysis of shells under totally arbitrary loads, as well as imperfection studies on actual shells with measured imperfections [11]. Unfortunately, the original deck of cards for SATANS-II was destroyed. Professor Johann Arbocz of CALTECH had a listing of SATANS-II and punched a deck of cards with the changes to SATANS-I given in that listing. A copy of this deck was sent to Professor Ball. These cards have been added by the author to the original SATANS-I described by Ryan [10] and a complete version of SATANS-II has been reconstructed. SATANS-IIA is a modification by the author of the reconstructed SATANS-II program. A listing of SATANS-IIA can be found in Appendix A. The listing contains an example problem for the dynamic analysis of a clamped, truncated cone subjected to an impulsive loading which is uniform along the meridian and varies in a cosine distribution over one-half of the circumference. This problem is a sample problem suggested by the Lockheed Missiles and Space Corp. [12]. A condensed version of the output from the example problem is given in Appendix B. Input data preparation for SATANS-IIA can be found in Appendix C. The basic users manual, which includes preparation of input subroutines and the theory of the program, is contained in Reference 3, which can be obtained through COSMIC (M70-10098, LAR-10736), or ASIAC [13]. A users manual which includes preparation and handling of imperfection data within the SATANS programs can be found in

Ref. [10]. The above information, along with the following discussion, will inform the user on the capabilities and proper use of SATANS-IIA.

The modification of the SATANS-II program to make its core requirement variable was accomplished by putting in a single dimension statement at the beginning of the program, with subsequent dimensioning within the subroutines to only the first element of the vector or matrix. This is a convenient feature of the FORTRAN-IV language in which the program is written. The actual vector and matrix sizes are transmitted to the subroutines by an individual parameter list. Construction of the initial dimension statement and core request size is as follows:

The basic size of the program on the IBM-360/67 Digital Computer, without the initial dimension statement, is 272,000 bytes. This figure includes approximately 19,000 bytes of buffer space required for execution. Within the main dimension statement are fifteen variables. However, only three parameters are needed to specify the sizes of these fifteen variables.

Let a= The number of stations along the meridian of the  
shell times the number of harmonics considered.  
Let b= a, plus two fictitious stations times the number  
of harmonics considered.  
Let c= The number of harmonics considered.

The main dimension statement would then be constructed as,

```
DIMENSION P(4,4,a), DEE(4,4,a), DST(4,4,a), X(4,a),  
          PHIXB(a), PHITB(a), Z(4,b), ZO(4,b),  
          Z2(4,b), Z3(4,b), ZDOT(4,b), IS(99,c),  
          JS(99,c), ID(99,c), JD(99,c)
```

The 99's above limit the user to 99 harmonics in any one run and an unlimited number of meridional stations. The core requirement for the general case would be,

$$272,000 + 216a + 80b + 1584c = \text{bytes of core required.}$$

For a sample calculation of the core requirements consider the example of a spherical cap with 40 stations along the meridian, and an asymmetric analysis with two harmonics. Therefore,

$$a = 40(\text{stations}) \times 2(\text{harmonics}) = 80$$

$$b = 80 + 2 \times 2(\text{harmonics}) = 84$$

$$c = 2(\text{harmonics})$$

Thus, for the variables P, DEE, DST,

$$3 \times (4 \times 4 \times 80) = 3840 \text{ (words)} \times 4 = 15,360 \text{ bytes}$$

for the variable X,

$$4 \times (80) = 320 \text{ (words)} \times 4 = 1280 \text{ bytes}$$

for the variables PHIXB, PHITB,

$$2 \times (80) = 160 \text{ (words)} \times 4 = 640 \text{ bytes}$$

for the variables Z, ZO, Z2, Z3, ZDOT,

$$5 \times (4 \times 84) = 1680 \text{ (words)} \times 4 = 6720 \text{ bytes}$$

lastly, for the variables ID, JD, IS, JS,

$$4 \times (99 \times 2) = 792 \text{ (words)} \times 4 = 3168 \text{ bytes}$$

Therefore, the total size of the main dimension statement would be 27,168 bytes. This figure would be rounded up to the nearest even thousand bytes, i.e. 28,000 bytes. Finally, the core requirement for this example problem would be

$$272,000 + 28,000 = 300,000 \text{ bytes.}$$

### III. IMPROVED POLE ROUTINE

The SATANS code is based upon Sander's geometrically nonlinear equations under the conditions of small strains and moderately small rotations. The formulation is in four second order nonlinear partial differential equations in terms of  $U$ ,  $V$ ,  $W$ , and  $M_s$ , where  $U$ ,  $V$ , and  $W$  are the meridional, circumferential and normal displacements respectively, and  $M_s$  is the meridional bending moment. The nonlinear partial differential equations in the coordinates  $s$ ,  $\theta$ , and  $t$  are reduced to uncoupled sets of linear differential equations in  $s$  and  $t$  by expanding the variables in trigonometric series in the circumferential coordinate  $\theta$ , and treating the nonlinear terms as pseudo loads. The first and second derivatives in the meridional coordinate  $s$  are replaced by the conventional central finite difference approximations, i.e.

$$\{z\}'_i = 1/2\Delta (\{z\}_{i+1} - \{z\}_{i-1}) \quad (1)$$

and

$$\{z\}''_i = 1/\Delta^2 (\{z\}_{i+1} - 2\{z\}_i + \{z\}_{i-1}) \quad (2)$$

where  $\{z\}_i$  is the vector of  $U$ ,  $V$ ,  $W$ , and  $M_s$  at the  $i^{\text{th}}$  station,  $\Delta$  is the uniform dimension between stations, and primes denote partial derivatives with respect to  $s$ . Applying these approximations to the governing set of domain

equations leads to

$$[C]_i \{z\}_{i-1} + [B]_i \{z\}_i + [A]_i \{z\}_{i+1} = \{g\}_i \quad (3)$$

When the shell does not have a pole, fictitious stations one increment off of the shell are introduced at each end. Both the governing domain equations and the boundary conditions are applied at the two boundary points. Thus, all finite difference approximations to the derivatives, including those of the boundary conditions, are of order

$\Delta^2$ . However, prior to the development of SATANS-IIA, the treatment of the conditions to be applied at a pole at either end of a shell was handled by a simple Euler forward or backward difference approximation to the first derivative, with truncation error of order  $\Delta$ . For example, for a pole at  $s = 0$ , where  $i = 1$ , the first derivative at the pole was approximated with

$$\{z\}'_1 = 1/\Delta (\{z\}_2 - \{z\}_1). \quad (4)$$

At the time this procedure for handling the pole conditions was developed (1967) it was thought that this would not significantly alter the solution. However, it has since been discovered that such is not the case.

For the new pole routine, an expanded forward difference approximation of order  $\Delta^2$  is used at  $s = 0$  which takes into account the two stations after the pole, instead of just one station after the pole as in the Euler scheme. This approximation is

$$\{z\}'_1 = 1/2\Delta (-3\{z\}_1 + 4\{z\}_2 - \{z\}_3). \quad (5)$$



The conditions to be imposed upon the dependent variables at a pole are derived in Reference 14. They are :

$$\text{For } N = 0, \quad u_1 = v_1 = w'_1 = m'_s = 0.$$

Applying equation (5), these conditions can be put into the matrix form

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & -3 & 0 \\ 0 & 0 & 0 & -3 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_1 + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 4 & 0 \\ 0 & 0 & 0 & 4 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_2 + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & -1 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_3 = 0.$$

where the above 3 matrices are DL, DG, and DF within the SATANS programs.

$$\text{For } N = 1, \quad u_1 \pm v_1 = u' = w = m_s = 0,$$

where the plus sign applies at an initial pole, and the minus sign at a final pole. The matrix form for these conditions is

$$\begin{bmatrix} -3 & 0 & 0 & 0 \\ 1 \pm 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_1 + \begin{bmatrix} 4 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_2 + \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_3 = 0.$$

$$\text{For } N=2, \quad u = v = w = m'_s = 0$$

the matrix form is

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & -3 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_1 + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 4 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_2 + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_3 = 0.$$

$$\text{For } N > 2, \quad u = v = w = m_s = 0$$

and  $DL =$  identity matrix,  $DG = DF =$  null matrices.

The solution procedure in SATANS is an elimination scheme and starts with

$$\{z\}_1 = - [P]_1 \{z\}_2 + \{x\}_1, \quad (6)$$

where the values in  $[P]_1$  based upon the Euler approximation are defined in Reference 14. The higher order approximation defines a new  $[P]_1$ . This new  $[P]_1$  is obtained by simultaneously solving the pole conditions

$$[DL] \{z\}_1 + [DG] \{z\}_2 + [DF] \{z\}_3 = \{0\}, \quad (7)$$

and the domain equation at station 2 next to the pole

$$[C]_2 \{z\}_1 + [B]_2 \{z\}_2 + [A]_2 \{z\}_3 = \{g\}_2, \quad (8)$$

to eliminate  $\{z\}_3$ . Thus,

$$\{z\}_3 = [A]_2^{-1} (\{g\}_2 - [C]_2 \{z\}_1 - [B]_2 \{z\}_2). \quad (9)$$

Substituting equation (9) into equation (7) gives

$$[DL] \{z\}_1 + [DG] \{z\}_2 + [DF] [A]_2^{-1} (\{g\}_2 - [C]_2 \{z\}_1 - [B]_2 \{z\}_2) = 0. \quad (10)$$

Combining like coefficients of the  $\{z\}$  vector leads to

$$([DL] - [DF] [A]_2^{-1} [C]_2) \{z\}_1 + ([DG] - [DF] [A]_2^{-1} [B]_2) \{z\}_2 = - [DF] [A]_2^{-1} \{g\}_2. \quad (11)$$

Finally, solving for  $\{z\}_1$  yields

$$\begin{aligned} \{z\}_1 &= - [DL - DF \times A_2^{-1} \times C_2]^{-1} [DG - DF \times A_2^{-1} \times B_2] \{z\}_2 \\ &+ [DL - DF \times A_2^{-1} \times C_2]^{-1} [-DF \times A_2^{-1}] \{g\}_2. \end{aligned} \quad (12)$$

Thus,  $[P]_1 = - [DL - DF \times A_2^{-1} \times C_2]^{-1} [DG - DF \times A_2^{-1} \times B_2]$  and  $\{x\}_1 = [DL - DF \times A_2^{-1} \times C_2]^{-1} [-DF \times A_2^{-1}] \{g\}_2$ . The new  $[P]_1$  matrix has been placed into the "PMATRIX" subroutine of SATANS-IIA and the new  $\{x\}_1$  vector has been placed in the "FORCE" subroutine.

A listing of the pole routine may be found in Appendix D. To incorporate this new routine into a SATANS-I or-II program, first proceed to the "PMATRIX" subroutine and remove the fifteen cards that are between, but not including, "IF(NN.GT.2) GO TO 90" and "11 CONTINUE". These cards are located after statement number "14" and just before statement number "11". Replace the cards removed by the ones listed in Appendix D which read from "C IN PMATRIX" to "90 M3=MN". Then proceed to the "FORCE" subroutine and remove statement number "10". Replace statement number "10" with the nine cards listed in Appendix D which read from "C IN FORCE" to "DO 11 I= 1,4". Also place "COMMON /IBL5/IBCINL, IBCFNL" into the common area of the "FORCE" subroutine.

This completes the implementation of the new pole routine into either SATANS-I or II.

#### IV. PROBLEM DESCRIPTION

The geometry of the shallow spherical shell used in this study is identical to that used in Reference 1. Briefly, the shallow shell can be specified by the non-dimensional parameter  $\lambda$ , where

$$\lambda = 2[3(1 - \nu^2)]^{1/4} (H/h)^{1/2}. \quad (1)$$

$H$  is the rise of the shell,  $h$  is the thickness, and  $\nu$  is Poisson's ratio. The mass density of the shell is  $m$ . All shells analyzed had the following dimensions;

Radii of Curvature	$R = R_\theta = 250$ inches
Thickness	$h = 0.25$ inches
Modulus of Elasticity	$E = 30,000,000$ psi
Poisson's Ratio	$\nu = 0.3$

All buckling pressures obtained will be listed as a percent of the classical buckling pressure of a complete sphere,  $q_0$ , where

$$q_0 = [2E(h/R_s)^2] / [3(1 - \nu^2)]^{1/2} \quad (2)$$

Forty stations were used over the meridian. The nondimensional time increment  $\delta t$ , where

$$t = T / (R_s^2 m / E)^{1/2}, \quad (3)$$

was taken as 0.05 for 3000 time steps, which is a total nondimensional time of 150. In addition, the axisymmetric analysis was repeated with a larger time step of  $\delta t = 0.2$  for a total time of 600. In this study  $m$  was selected such that  $t$  is equal to  $T$ . The necessity for the long response time is explained in Reference 6.

In the axisymmetric analysis only the  $N = 0$  harmonic is considered. However, in the asymmetric analysis a second harmonic is excited by applying an incremental load in that harmonic. In addition, analyses of the shells  $\lambda = 6, 7.5$ , and 11 were made using five harmonics. The step pressure load for the axisymmetric harmonic is

$$\{q^{(0)}\} = P q_0 \{1\}, \quad (4)$$

and the step pressure load for the asymmetric second harmonic is

$$\{q^{(n)}\} = P q_0 \xi^{(n)} \{1\}, \quad (5)$$

where  $n > 0$ , and  $\xi^{(n)}$  is taken as 0.0001. The value taken for the second harmonic in the asymmetric analysis was the same as the critical harmonic for the static buckling analysis presented by Stilwell and Ball [2]. When there was an uncertainty as to which was the critical static harmonic the two harmonics in question were both tested. Run times using SATANS-IIA with a two-harmonic analysis for 3000 time steps and 40 stations on the meridian took an average of 28 minutes on the IBM 360/67.

The parameter used to determine the minimum load at which dynamic buckling occurs is the peak value of  $\bar{V}$ , called



$\bar{V}_{MAX}$ , where  $\bar{V}$  is defined as

$$\bar{V} = \int_0^{r_0} r w^{(0)} dr / \int_0^a r \xi dr \quad (6)$$

$r$  is the normal distance from the axis to the shell,  $r_0$  is the maximum value of  $r$ ,  $w^{(0)}$  is the normal displacement of the axisymmetric response and  $\xi$  is the vertical distance from the base plane to the undeformed shell. The  $\bar{V}$  is a measure of the volume of the shell deformation. The Fortran statements computing  $\bar{V}$  and  $\bar{V}_{MAX}$  are given in Appendix E.

When working a problem that requires these calculations the nineteen cards are inserted directly into the "DYNAMIC" subroutine right after the "IF" statement that calls the "OUTPUT" subroutine.

For convenience, the response in each asymmetric harmonic is also measured using equation (6), with  $w^{(0)}$  replaced with  $w^{(n)}$ . The parameter  $\bar{V}$  for the asymmetric harmonics does not represent a volume of deformation as it does for the axisymmetric harmonic. It can, however, be used to indicate the relative excitation of the asymmetric harmonics.

The buckling criterion for both the axisymmetric and the asymmetric dynamic buckling analysis defines the critical load as that load  $P$  where a very small increase in  $P$  causes a very large increase in  $\bar{V}_{MAX}$ . This is the same criterion

as that used in Ref. [1].

## V. RESULTS AND DISCUSSION

### A. STATIC AXISYMMETRIC BUCKLING ANALYSIS

Table I presents the new results from the static axisymmetric buckling analyses for  $\lambda = 4$  through 13 using the new pole routine. The two upper curves in Figure 1 present a comparison of the new results obtained by SATANS-IIA with those obtained by Stilwell and Ball [2] using the SATANS-I program. As can be seen in this figure, fairly significant changes in the buckling load occurred in the neighborhood of  $\lambda = 4, 5$ , and 9; and somewhat smaller differences occurred in the region  $\lambda = 10$  through 13. The upper data points in Figure 2 present the comparison of the new results from SATANS-IIA with those obtained by Huang [4]. This comparison shows a very good agreement between the two sets of results, except for the largest values of  $\lambda$ . The new results have eliminated the differences that existed between the SATANS-I results and Huang's results.

### B. DYNAMIC AXISYMMETRIC BUCKLING ANALYSIS

Figure 3 presents the new results for the peak value of  $\bar{V}_{MAX}$  versus P for the various values of  $\lambda$  tested. Table II presents all of the new results for the dynamic axisymmetric buckling load. These loads are selected from figures constructed just like Figure 3. In every case,

except for  $\lambda = 4$ , a value of  $P$  slightly above the  $P_{CRIT}$  value caused a  $\bar{V}_{MAX}$  indicative of buckling, as well as a nonconvergence of the iterative solution procedure.

The lower two curves of Figure 1 present a comparison versus  $\lambda$  of the new axisymmetric dynamic buckling results with the previous buckling results obtained by Ball and Burt [1]. In every case the new critical pressure is lower than the critical pressure obtained using the Euler approximation at the pole.

The lower data points of Figure 2 present a comparison of the new results with those obtained by Huang [5], by Stephens and Fulton [6], and by Stricklin [8]. Just as in the case of the static axisymmetric buckling analysis, the new results compare much more favorably with the other results than did the results of Reference 1. It's interesting to note that the new results now tend to be slightly lower than the other results, whereas the results of Reference 1 were higher for almost all values of  $\lambda$ .

### C. DYNAMIC ASYMMETRIC BUCKLING ANALYSIS

Table III presents the new results for the critical pressures obtained from the dynamic asymmetric analysis. The second harmonics, or critical static harmonics, used in the analyses are also presented in Table III. A comparison of the critical pressures from the asymmetric analyses, Table III, with the critical pressures from the axisymmetric analyses, Table II, reveals that only the shell  $\lambda = 6$  buckled at a load below the axisymmetric buckling load. For the shell  $\lambda = 7$  the critical buckling load was slightly

larger when asymmetric motion was considered. In all other cases the buckling was not influenced by the presence of the second harmonic. These new buckling results and those by Ball and Burt [2] are plotted in Figure 4. The new results can be seen to be significantly different from the SATANS-I results, where the asymmetric buckling loads were lower than the axisymmetric loads for five out of the ten values of tested.

Except for  $\lambda = 6$  and 7, the relationship between  $\bar{V}_{MAX}$  and P for the  $N=0$  harmonic, in the two-harmonic analyses, was found to be essentially identical to the relationship found in the axisymmetric buckling analysis shown in Figure 3. Table IV A presents the  $\bar{V}_{MAX}$  versus P data for both the  $N=0$  harmonic and the second harmonic, for all values of  $\lambda$  tested, except for  $\lambda = 6$ . Note that, except for  $\lambda=7$  and 11,  $\bar{V}_{MAX}$  for the asymmetric harmonic is generally very small, even when the  $\bar{V}_{MAX}$  for the  $N=0$  harmonic indicates that the shell has buckled. Thus, except for the shells  $\lambda = 6$  and 7, the presence of the asymmetric motion does not influence the axisymmetric motion, and except for the shells  $\lambda = 6, 7$  and 11 the asymmetric motion is very small prior to buckling in the axisymmetric harmonic.

A more detailed analysis of the shell  $\lambda = 6$  has been conducted since it was the only shell that revealed any significant axisymmetric sensitivity to asymmetric motion. This shell was studied using two two-harmonic analyses ( $N=0, 1$  and  $N=0, 2$ ) and a five-harmonic analysis ( $N=0, 1, 2, 3$ , and 4). Figure 5 and Tables IV B and IV C contain values of  $\bar{V}_{MAX}$  versus P for both of the asymmetric harmonics,  $N=1$

and  $N=2$ , in the two two-harmonic analyses, as well as the values of  $\bar{V}_{MAX}$  for the axisymmetric harmonic,  $N=0$ . Figure 6 and Table IV D present the values of  $\bar{V}_{MAX}$  versus  $P$  for the  $N=0,1,2,3$ , and 4 harmonics from the five-harmonic study. A comparison of the critical buckling load predicted from the results of the two two-harmonic analyses in Figure 5 with the critical load from the five-harmonic analysis obtained from Figure 6 shows that the presence of the additional harmonics results in the shell buckling at a slightly lower load (0.50), with significant motion in the  $N=1$  harmonic instead of the  $N=2$  harmonic (see the nonconverged solution at  $P=0.51$ ), which is the critical harmonic for static asymmetric buckling. Studies using five harmonics have also been conducted for  $\lambda=7.5$  and  $\lambda=11$ . As can be seen in Table IV D the critical harmonic for  $\lambda=7.5$  remained  $N=3$ ; however, significant motion occurred in that harmonic at  $P=.41$  and  $.44$ . In the case of  $\lambda=11$ , relatively large asymmetric motion occurred in the asymmetric mode of  $N=5$  vice 6 at a value of  $P=.46$ .

The comparison of the new results for the critical pressure for dynamic asymmetric buckling with those obtained analytically by Stricklin [8], by Akkas [9], and experimentally by Lock et al [7] is illustrated in Figure 7. The comparison reveals an agreement with Stricklin in every case, in general a higher value of  $P_{CRIT}$  than those obtained by Akkas, and most importantly a very good agreement with Lock's experimental results.

When making the comparison between the new results and those obtained by Akkas, it is necessary to look at the differences in the problem solution parameters used in the two studies. For example, buckling results obtained from SATANS-IIA using the same time increment as used by Akkas,

$\delta t = .2$  for 3000 time steps, were significantly higher than those using the time step of  $\delta t = .05$  for many values of  $\lambda$ . Furthermore, the new results had, in some cases, instances of buckling occurring as far out in time as 130. Akkas, to shorten computer run times, observed the cap only for a time of less than 5. Furthermore, only the harmonics  $N = 1$  or 2 or 3 were studied by Akkas for shells  $\lambda = 5$  through 12. If the critical harmonic is not studied, the predicted load will be too high. Thus, it appears that Akkas' lower bound loads may not be true lower bounds.

Two additional features of the shell response should be noted. First, shells  $\lambda = 6, 7.5$ , and 11 exhibited a non-buckled response in the axisymmetric harmonic to a load larger than the defined critical buckling load. This can be seen in Tables IV A and IV C. Second, and most importantly, the buckling load proposed by Ball and Burt [1], and used here, defines buckling to occur when the  $\bar{V}_{MAX}$  in the axisymmetric harmonic undergoes a large change due to a small change in  $P$ . Another criterion for dynamic buckling in the asymmetric analysis discussed in Reference 1 is to define the buckling load as that threshold load that initiates significant growth in the asymmetric harmonic. Re-examination of the  $\bar{V}_{MAX}$  versus  $P$  data in Table IV A through D reveals that shells  $\lambda = 6, 7$ , and 11 exhibited relatively large asymmetric motion at loads smaller than the defined buckling load when compared with other  $\bar{V}_{MAX}$  values for those shells, even though the numbers themselves were small when compared with the axisymmetric harmonic. Shells  $\lambda = 7.5$  and 12 appear to be borderline cases. If the alternate criterion for buckling is used, the critical buckling loads for shells  $\lambda = 6, 7$ , and 11 become 0.47, 0.45, and 0.45, respectively. The shells  $\lambda = 7.5$  and 12 could have buckling



loads as low as 0.40 and 0.44, respectively. These values are more conservative than the definition based upon axisymmetric response. These five shells are the same five shells that exhibited an asymmetric buckling load lower than the axisymmetric buckling load in Reference 1.

## VI. SUMMARY AND CONCLUSIONS

A digital computer program for the geometrically nonlinear analysis of totally arbitrarily loaded shells of revolution (SATANS-II) was modified to more accurately account for the conditions at the pole of the shell. This program, called SATANS-IIA, was used to determine the buckling load of shallow spherical shells of various sizes when subjected to static axisymmetric, dynamic axisymmetric, and dynamic nearly axisymmetric step-pressure loads of infinite duration. The cap sizes ranged from  $\lambda = 4$  to 13 including  $\lambda = 7.5$ . A comparison was made between the new buckling results with the improved pole handling routine and the results that did not have the new pole routine. The comparison revealed a significant change in buckling pressures, due solely to the change from an order  $\Delta$  finite difference approximation of the first derivatives at the pole to an approximation of order  $\Delta^2$ . These new critical pressures are in very good agreement with the results from other studies of the same spherical shells. This good agreement with other results, which came about as a result of the modification of the pole handling routine, is a strong indication that the manner in which the pole condition is handled is vital to the accuracy of the solutions obtained.

In the asymmetric analysis, two harmonics were included for most of the shells; the axisymmetric harmonic and one asymmetric harmonic. Five-harmonic analyses were conducted for three of the shells. Two buckling criteria for the

asymmetric analysis were considered. One defined buckling as that threshold load that caused a large increase in a deformation parameter,  $\bar{V}_{MAX}$ , in the axisymmetric harmonic.

The other, more conservative than the first, defined buckling as that threshold load that caused a large increase in the  $\bar{V}_{MAX}$  value for the asymmetric harmonic. Both values have been presented.

The new static axisymmetric, dynamic axisymmetric, and even the dynamic asymmetric critical buckling pressure loads appear to be fairly reliable results for perfect, shallow shells. The effect of realistic imperfections remains to be determined.

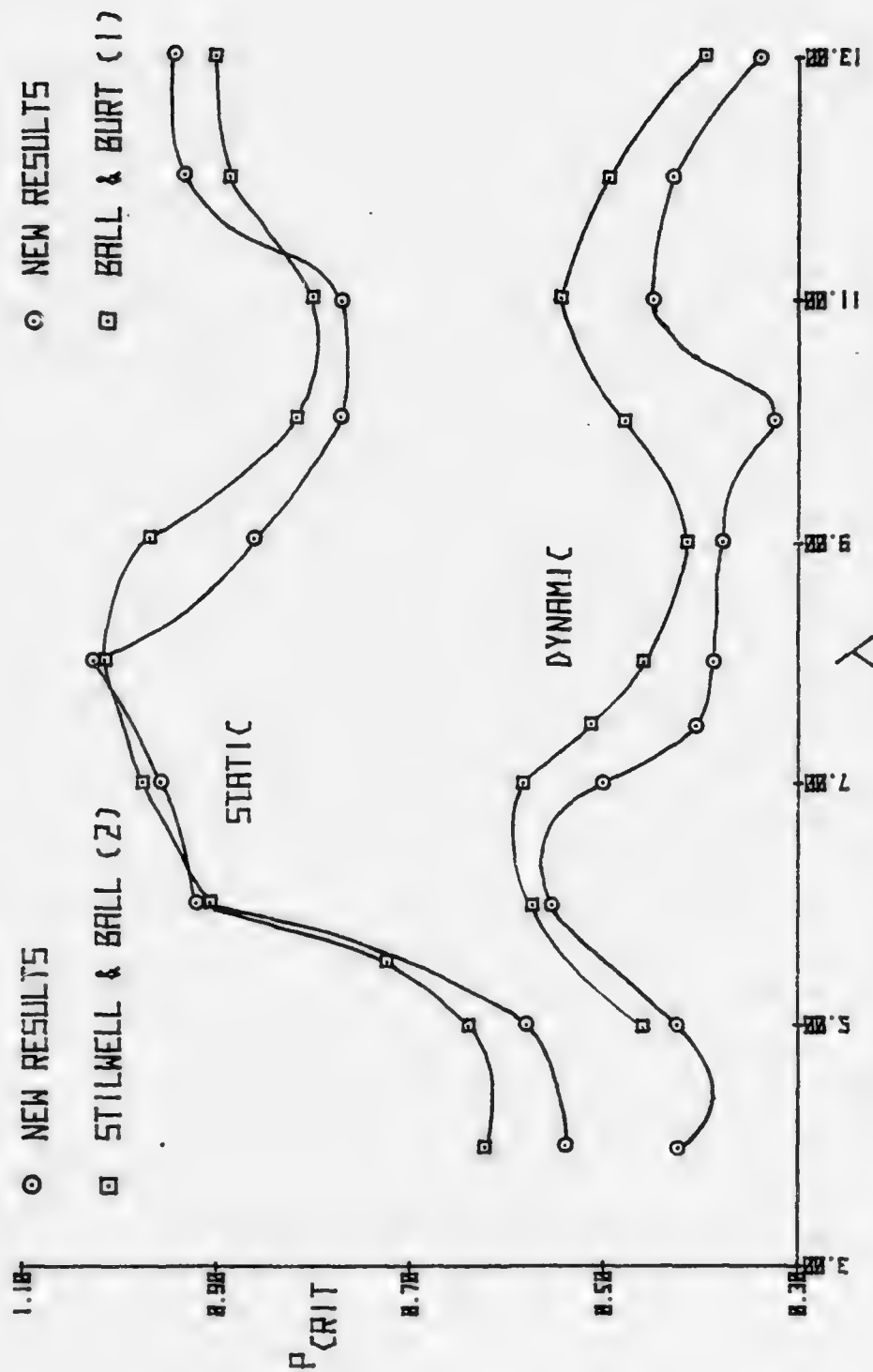


Figure 1 - CRITICAL STEP-PRESSURE LOAD VERSUS  $\lambda$   
AXISYMMETRIC (SATANS-I) VERSUS SATANS-IIA)

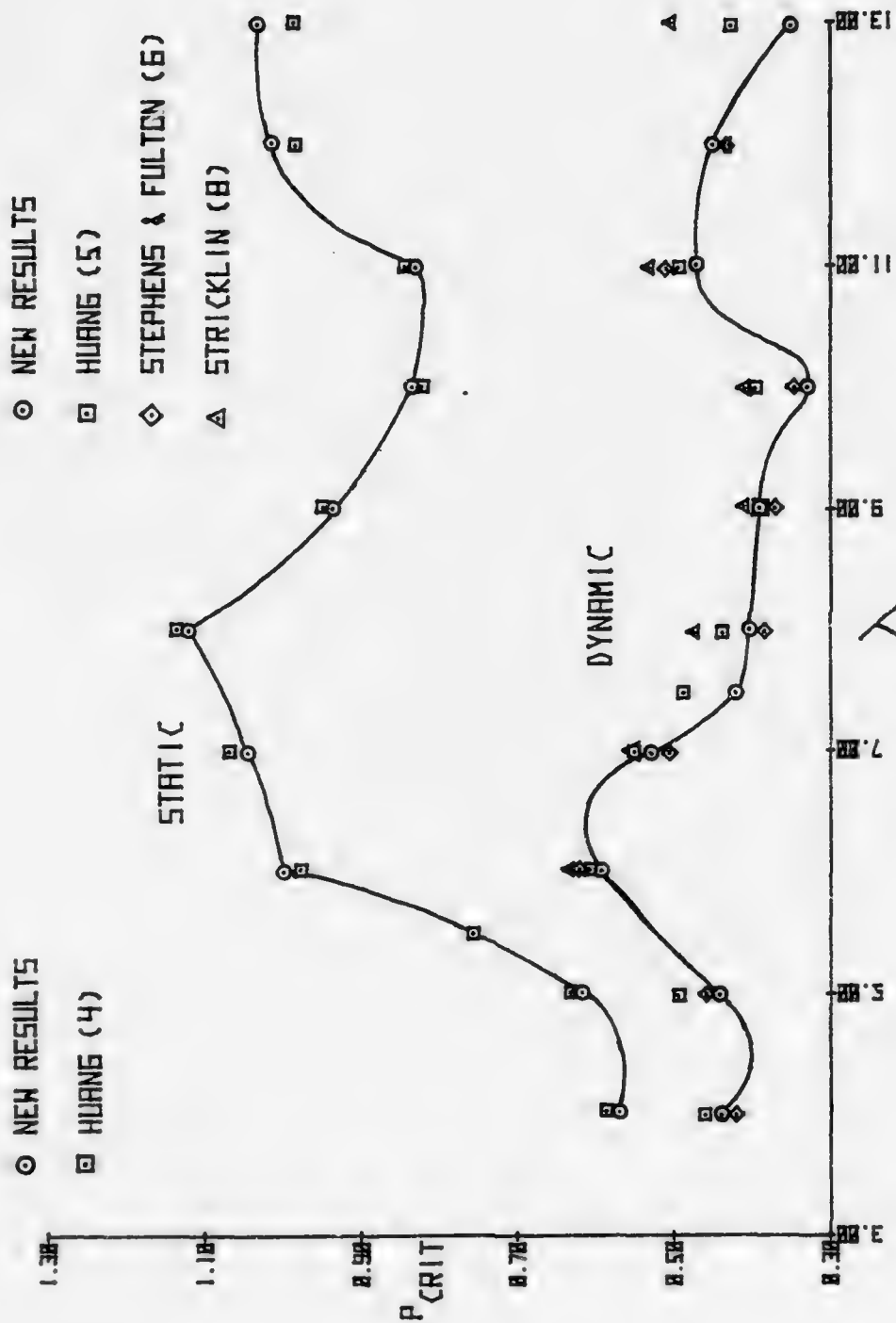


Figure 2 - CRITICAL STEP-PRESSURE LOAD VERSUS  $\lambda$   
AXISYMMETRIC (SATANS-IIA VERSUS ALL OTHERS)

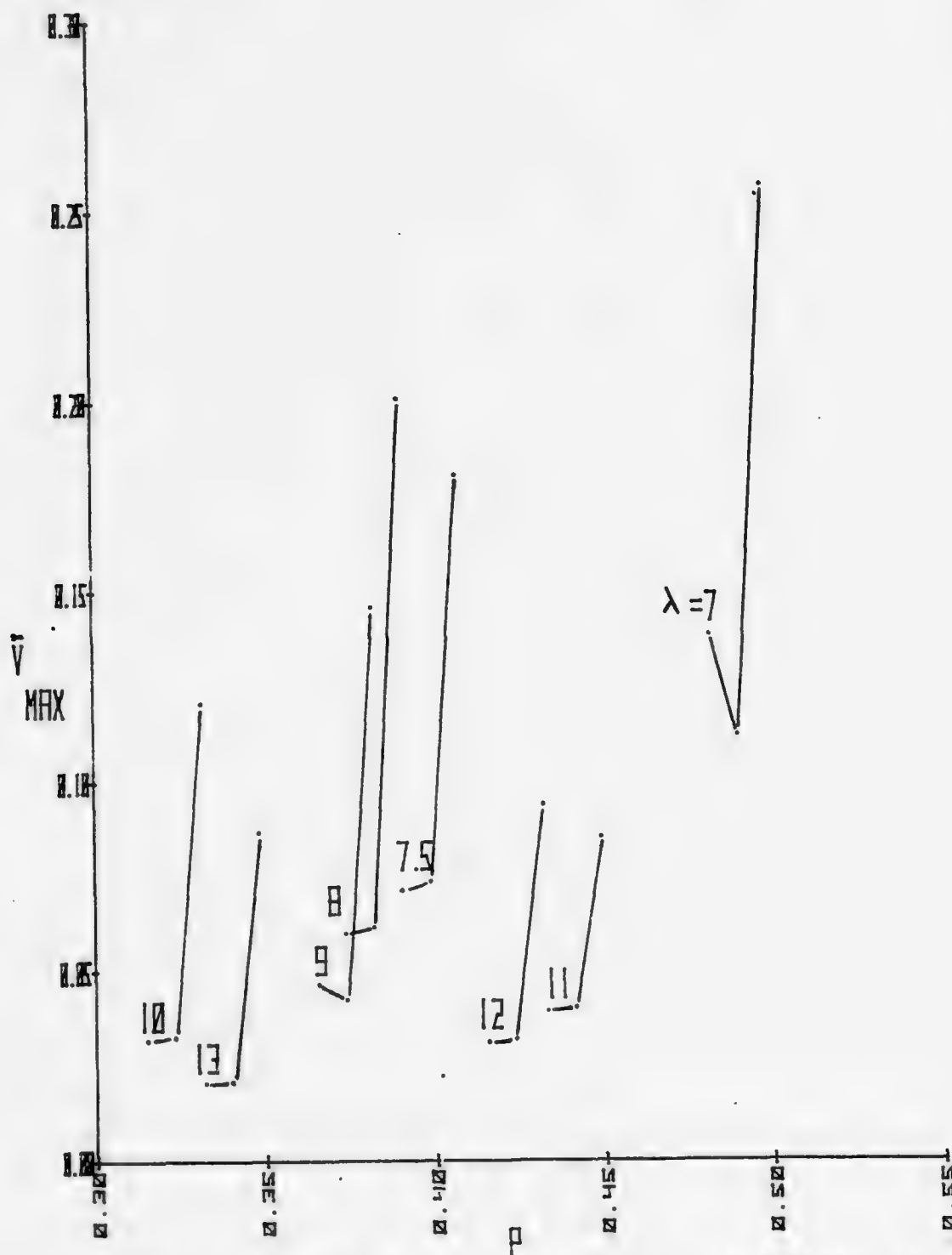


Figure 3 - PEAK DEFLECTION VERSUS P, AXISYMMETRIC AND ASYMMETRIC CASES FOR VARIOUS VALUES OF  $\lambda$  (SATANS-IIA)

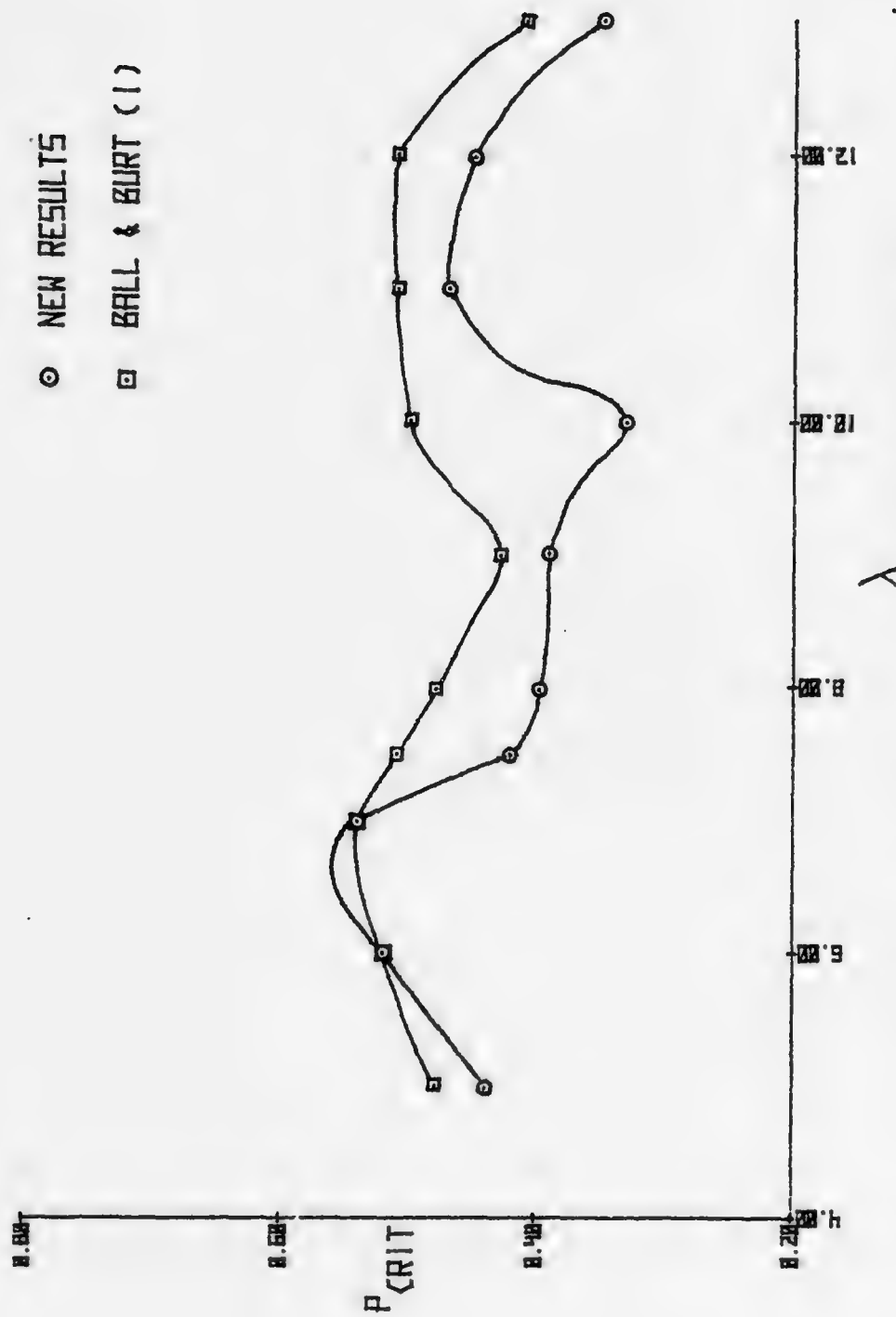
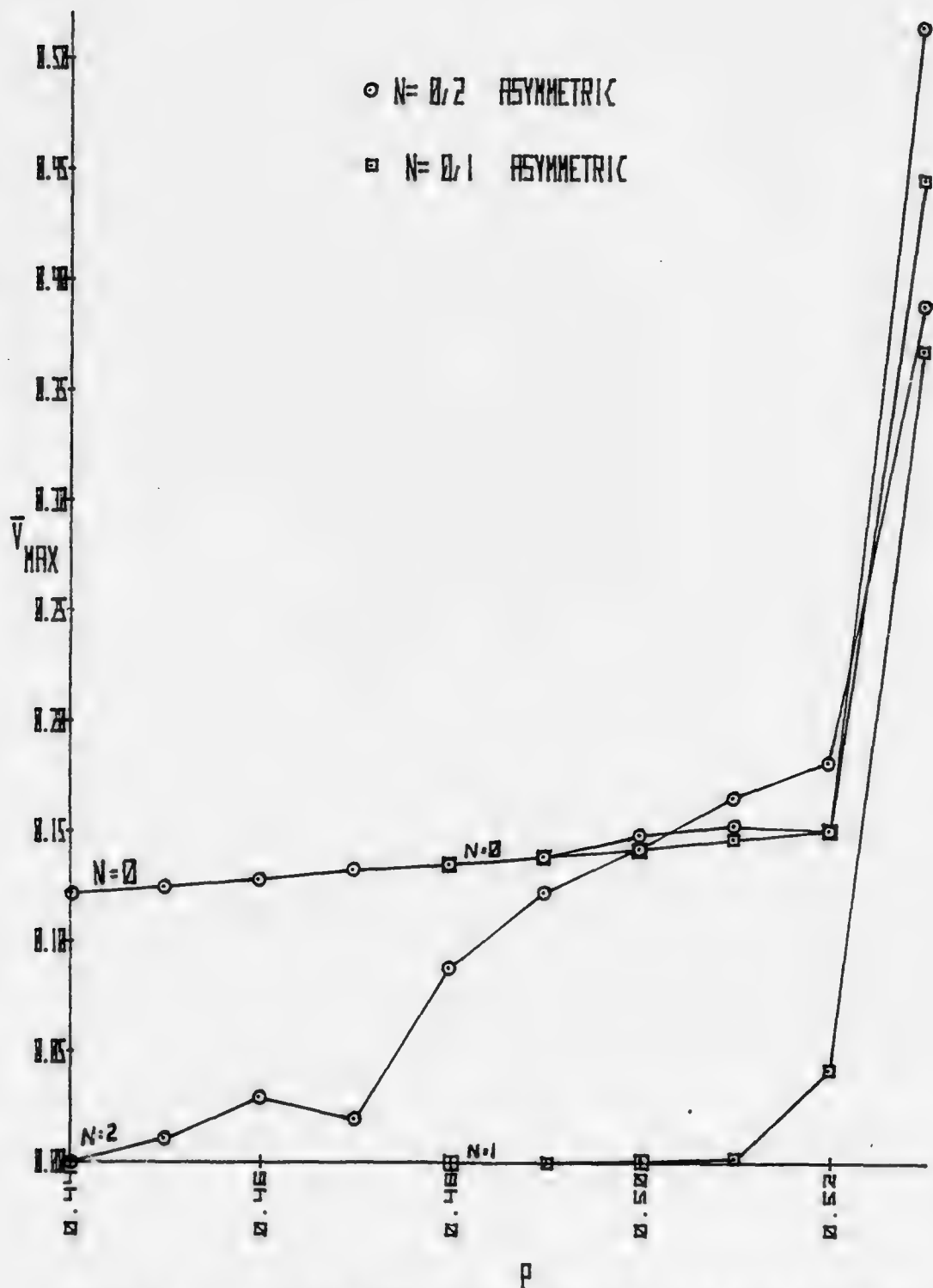


Figure 4 - CRITICAL STEP-PRESSURE LOAD VERSUS  $\lambda$   
ASYMMETRIC ANALYSES (SATANS-I VERSUS SATANS-IIA)





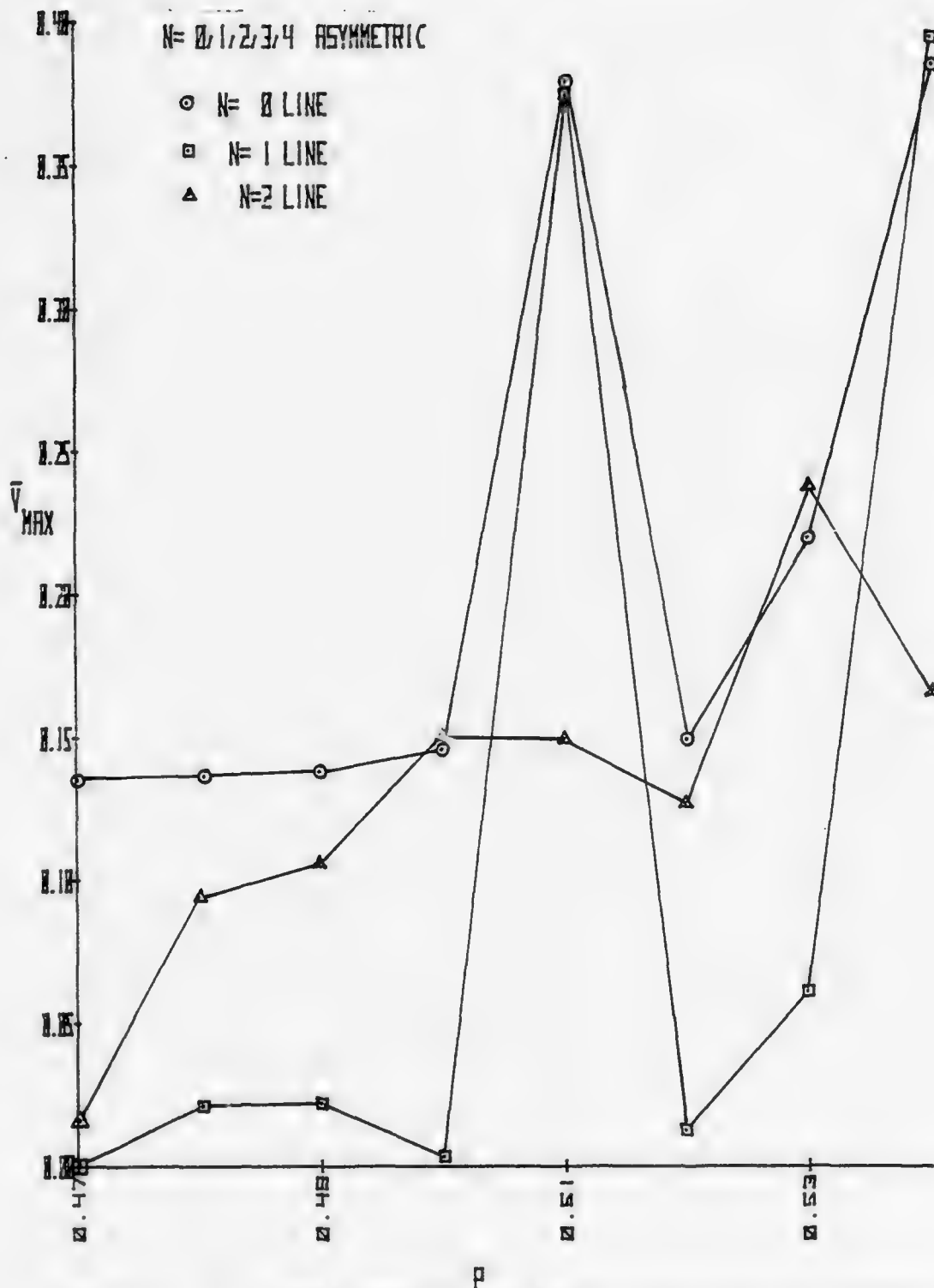


Figure 6 - PEAK DEFLECTION VERSUS P FOR THE ASYMMETRIC ANALYSES OF  $\lambda = 6$  ( $N=0, 1, 2, 3$ , AND 4, ONLY  $N=0, 1$ , AND 2 PLOTTED)

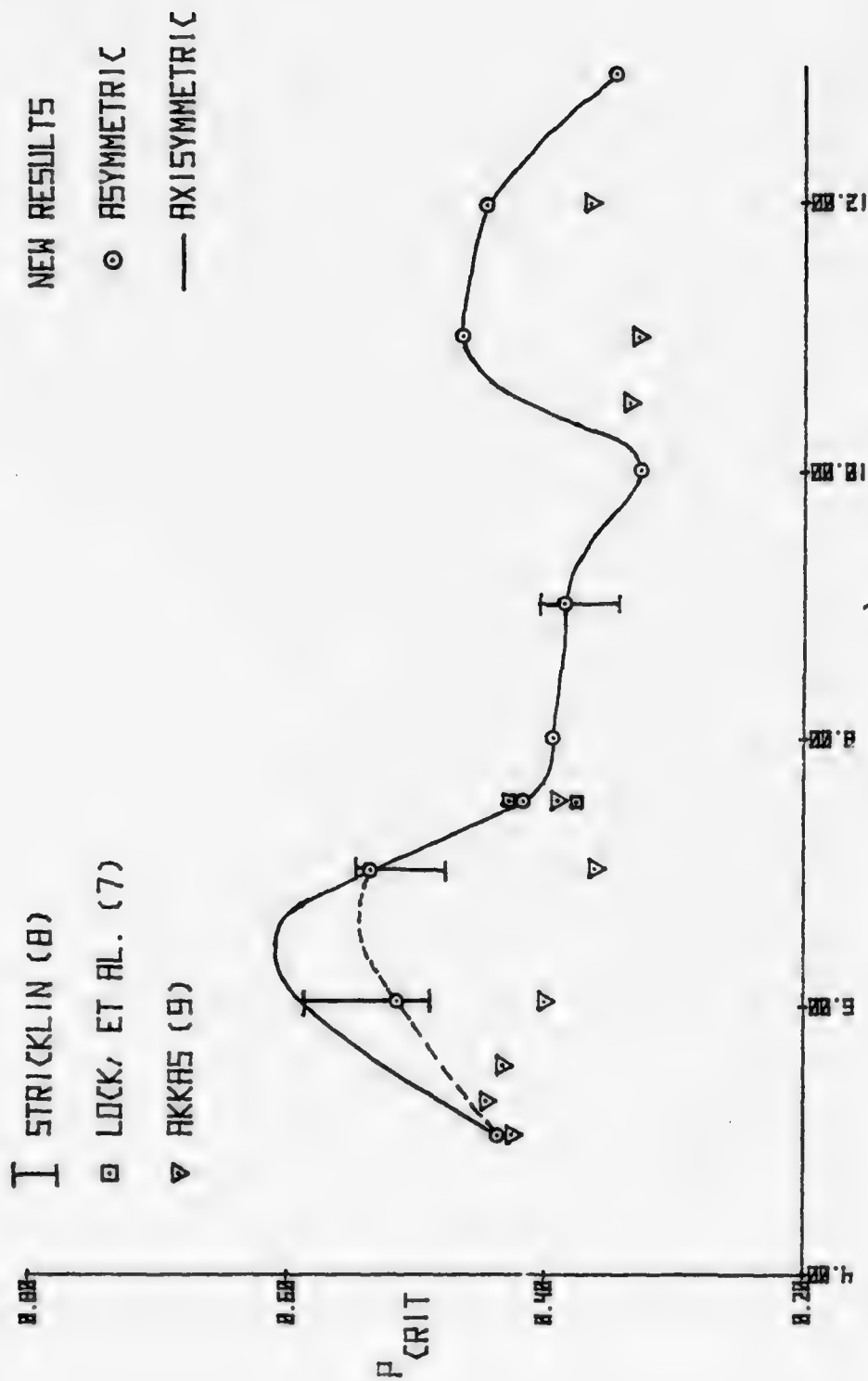


Figure 7 - CRITICAL STEP-PRESSURE LOAD VERSUS  $\lambda$   
ASYMMETRIC ANALYSES (SATANS-IIA VERSUS ALL OTHERS)

## A. TABLES

1. TABLE I Critical pressure loads from the static axisymmetric analyses.

$\lambda$	4	5	6	7	8	9	10	11	12	13
$P_{CRIT}$	.568	.616	1.0	1.048	1.12	.936	.832	.832	1.016	1.032

2. TABLE II Critical step-pressure loads from the axisymmetric dynamic analyses.

$\lambda$	4	5	6	7	7.5	8	9	10	11	12	13
$P_{CRIT}$	.45	.44	.59	.53	.42	.40	.39	.33	.47	.45	.35

3. TABLE III Critical step-pressure loads from the dynamic asymmetric analyses and critical asymmetric harmonics.

$\lambda$	5	6	7	7.5	8	9	10	11	12	13
$P_{CRIT}$	.44	.52	.54	.42	.40	.39	.33	.47	.45	.35
$N_{CRIT}$	1	2	3	3	4	5	6	7	8	9

4. TABLE IV Dynamic asymmetric analyses for  $\bar{V}_{MAX}$  versus

P.

1. TABLE IV A. Two-harmonic analyses for all values of  $\lambda$  except  $\lambda = 6$ .

$\lambda = 5$  N= 0 and 2

N= 0 and 1

P	.43	.44	.45	P	.44	.45
N= 0	.1659	.1676	.6606	N= 0	.1675	.6606
N= 2	.0004787	.0000566	.0687	N= 1	.0003145	.0687
				P	.46	
				N= 0	.7653	
				N= 1	.001092	

$\lambda = 7$ , N= 0 and 3

P	.45	.46	.47	.48	.49	.50	.52
N= 0	.09452	.09571	.09812	.1005	.1029	.1052	.1099
N= 3	.000889	.007456	.05052	.04323	.0279	.0335	.07488
P	.53	.54	.55				
N= 0	.1122	.1146	.2709				
N= 3	.05997	.06252	.03809				

$\lambda = 7.5$ , N= 0 and 3

P	.40	.41	.42	.43	.44	.45
N= 0	.0703	.07228	.07429	.2636	.07837	.2076
N= 3	.0001094	.001296	.0004304	.002754	.001188	.000338
P	.46					
N= 0	.200					
N= 3	.0003276					

$\lambda = 8, N = 0 \text{ and } 4$

P	.38	.39	.40	.41	.42	.43
N= 0	.05893	.0607	.0624	.1964	.1713	.1957
N= 4	.0000566	.0000703	.0000364	.0000333	.0000274	.0000299
P	.44					
N= 0	.2297					
N= 4	.0000326					

$\lambda = 9, N = 0 \text{ and } 4$

$N = 0 \text{ and } 5$

P	.38	.39	.40	P	.40
N= 0	.04738	.04875	.1576	N= 0	.05012
N= 4	.00003597	.00004635	.00004497	N= 5	.00008385

$\lambda = 10, N = 0 \text{ and } 5$

P	.32	.33	.34	.36	.38	.40
N= 0	.03239	.03347	.1086	.1217	.1288	.1235
N= 5	.0000281	.0000472	.00004125	.00002103	.0000449	.000114

$\lambda = 11, N = 0 \text{ and } 6$

P	.45	.46	.46	.48	.49	.50
N= 0	.03910	.04004	.04099	.09814	.04241	.08824
N= 6	.004595	.01332	.02232	.02864	.03955	.02813

$\lambda = 12, N = 0 \text{ and } 7$

P	.44	.45	.46
N= 0	.03236	.03316	.08633
N= 7	.00004214	.0004561	.00005158

$\lambda = 13, N = 0 \text{ and } 8$

P	.34	.35	.36	.38	.40
N= 0	.02119	.02185	.06637	.07844	.07381
N= 8	.00001148	.00001134	.000006607	.000008245	.000119

2. TABLE IV B. Two-harmonic analyses with  $N=0$  and 1,  
 $\lambda = 6$  only.

P	.48	.49	.50	.51	.52	.53
N= 0	.1350	.1385	.1421	.1460	.1499	.4453
N= 1	.0002797	.000195	.000245	.000926	.04081	.3668

3. TABLE IV C. Two-harmonic analyses with  $N=0$  and 2,  
 $\lambda = 6$  only.

P	.44	.45	.46	.47	.48	.49	.50
N= 0	.1218	.1250	.1276	.1320	.1350	.1385	.1479
N= 2	.000239	.0101	.0293	.01976	.08768	.1223	.1419
P	.51	.52	.53	.54	.55	.56	
N= 0	.1526	.1499	.5137	.5060	.2040	.5305	
N= 2	.1654	.1816	.3878	.3996	.2156	.3617	

4. TABLE IV D Five-harmonic analyses for selected  
shells.

$\lambda = 6$   $N=0,1,2,3$ , and 4

P	.47	.48	.49	.50	.51	.52	.53
N= 0	.1313	.1347	.1382	.1460	.3797	.1498	.2200
N= 1	.00021	.02108	.02215	.003676	.3743	.01276	.0616
N= 2	.0187	.0953	.1069	.1507	.1502	.1279	.2385
N= 3	.000181	.006237	.01437	.00163	.0405	.0123	.03978
N= 4	.0031	.04757	.05428	.04402	.05896	.0495	.064
P	.54						
N= 0	.3854						
N= 1	.3953						
N= 2	.1671						
N= 3	.05298						
N= 4	.0613						



$\lambda = 7.5$   $N = 0, 1, 2, 3, 4$  and 4

P	.40	.41	.42	.43	.44	.45
N= 0	.0703	.07228	.07429	.2592	.07837	.2544
N= 1	.00004855	.00004198	.00006093	.0002737	.0001167	.005952
N= 2	.0001164	.00007456	.0004184	.0000982	.000788	.0003188
N= 3	.0001277	.001187	.0004597	.0002853	.00107	.0003188
N= 4	.0008224	.0001898	.0002448	.0000526	.000280	.000134

$\lambda = 11$   $N = 0, 4, 5, 6,$  and 7

P	.45	.46	.47	.48	.49	.50
N= 0	.03910	.04004	.0499	.04195	.04291	.1040
N= 4	.0005759	.001263	.0009774	.001388	.002657	.001565
N= 5	.009568	.0140	.0124	.02239	.02759	.01548
N= 6	.002560	.007828	.02330	.02767	.02602	.02644
N= 7	.0001743	.0001486	.0002021	.01202	.02048	.02064

APPENDIX A

LISTING OF SATANS-IIA

```

C*****SAT000010
C THIS PROGRAM SERVES AS THE 'MAIN' PROGRAM, AND CALLS 'SATANS', *SAT000020
C AND CHECKS 'IRNAGN' TO SEE IF WE DESIRE ANOTHER RUN *****
C*****SAT000030
C*****
C DIMENSION P(4,4,124), DEE(4,4,124), DST(4,4,124), X(4,124), Z(4,122),
C 12C(4,132), Z2(4,132), Z3(4,132), ZCCF(4,132), IS(99,4), JS(95,4),
C 21C(99,4), JD(99,4), PHIXB(124), PHITB(124)
C CCMCN /BLRUN/ IRNAGN
C CCMCN /BLTHTA/ THETAM, COEFF
C CCNTINUE
C 1 CALL SATANS (P, DEE, DST, X, Z, Z0, Z2, Z3, ZDOT, IS, JS, ID, JD, PHIXB, PHITB)
C IF (IRNAGN.EQ.1) GO TO 1
C CALL FLYNVY
C STCF
C ENC

C*****SLEROUTINE GEOM
C*****THIS SUBROUTINE COMPUTES THE NONDIMENSIONAL GEOMETRY FUNCTIONS*****
C CF TPE SHELL*****
C*****
C REAL NU, LAM, LAM2, JAY, WT, LSD18, LSCIN, MASS
C CCMCN /BL4/ KMAX, KL
C CCMCN /BL8/ R(500), GAM(500), QMT(500)
C CCMCN /BL11/ OMXI(500), PHEE, t0, t2
C CCMCN /BL17/ DEEL
C CCMCN /BL20/ DEOMX(500)
C CCMCN /BL32/ TKN, ELAST, CHAR, SIGC
C CCMCN /BL102/ DELOAD
C CCMCN /BL103/ MASS(500)
C CCMCN /BLTHTA/ THETAM
C AKX=KMAX-1
C DEL=1./AKX
C TFE=ARSIN(2.2801/CHAR)
C CC 11 K=1, KMAX
C AK=K
C R(K)=(7.9455+(AK-1.)*(2.2801)/AKX)/CHAR
C GAM(K)=(2.2801/CHAR)/R(K)
C OMXI(K)=0.
C DEOMX(K)=0.
C CAT(K)=COS(THET)/R(K)
C MASS(K)=1.
C CCNTINUE
C 11 RETURN
C ENC

C*****SLEROUTINE BCB(K,B,CB,D,DD)*****
C*****
SAT000080
SAT000090
SAT000100
SAT000110
SAT000120
SAT000130
SAT000140
SAT000150
SAT000160
SAT000170
SAT000180
SAT000190
SAT000200
SAT000210
SAT000220
SAT000230
SAT000240
SAT000250

SAT000350
SAT000360
SAT000370
SAT000380
SAT000390

```

```

C *****
C      THIS SUBROUTINE COMPUTES THE NONDIMENSIONAL IN-PLANE AND
C      BENDING STIFFNESSES OF THE SHELL
C      REAL NU, LAM, LAM2, JAY, MT, LSD18, LSC1N
C      COMMON /BL15/ NU, U1(99), V1(99), W1(99), U2(99), V2(99), W2(99), U3(99),
C      V3(99), W3(99)
C      COMMON /BL17/ DEL
C      COMMON /BL32/ TKN, ELAST, CHAR, SIGC
C      E=1.C89C82
C      L=.C5C156E3
C      DE=C.
C      LL=0.
C      RETURN
C      END

```

```

C *****
C      SLRROUTINE PLOAD(K,Z)
C      *****
C      THIS SUBROUTINE ESTABLISHES THE NON-DIMENSIONAL FCURIER
C      COEFFICIENTS OF THE LOADS APPLIED TO THE SPELL
C      *****
C      REAL MASS
C      DIMENSION Z(4,1), MNMAX
C      COMMON /IBL1/ MNMAX
C      COMMON /IBL2/ NN(99), MNINIT
C      COMMON /IBL4/ KMAX, KL
C      COMMON /IBL8/ LSTEP, ITR
C      COMMON /BL3/ PR(99), PT(99)
C      COMMON /BL6/ SOE, OSE, ALOAD
C      COMMON /BL8/ R(500), GAM(500), QMT(500)
C      COMMON /BL32/ TKN, ELAST, CHAR, SIGC
C      COMMON /BL102/ DELGAD
C      COMMON /BL103/ MASS(500)
C      COMMON /BL17/ DEL/BL10C/TEEO, $DYNMC
C      COMMON /BLTHTA/ TFETAM, COEFF
C      RETURN
C      END

```

```

C *****
C      SLRROUTINE INITL (Z, ZC, Z2, Z3, ZCCT)
C      *****
C      THIS SUBROUTINE DESCRIBES THE INITIAL CONDITIONS FOR DYNAMIC CASES
C      *****
C      IMPLICIT LOGICAL*1 ($)
C      DIMENSION Z(4,1), ZC(4,1), Z2(4,1), Z3(4,1), ZCCT(4,1)
C      COMMON /IBL1/ MNMAX
C      COMMON /IBL2/ NN(55), MNINIT
C      COMMON /IBL4/ KMAX, KL
C      COMMON /IBL5/ MAXM
C      COMMON /IBL12/ KMAX1, KMAX2, NCONV
C      COMMON /BL6/ SOE, CSE, ALOAD

```















```

C      NTSSES, LOADING (PHYSICAL AND/OR THERMAL), AND INITIAL CCNTIDICNS. *SAT03730
C      IT CCNTRCLS PROBLEM SCLUTICAN PRCCEDURE. *SAT03740
C      ***** *SAT03750
C      INFLICIT LCGICAL#1 ($) MT, LSO18, LSCIN, MASS *SATC3760
C      REAL#4 NU, LAM, LAM2, JAY, DEE(4,4,1), DS1(4,4,1), X(4,1), Z(4,1), *SAT03770
C      DIMENSION P(4,4,1), Z3(4,1), ZDOOT(4,1), JS(99,1), IC(55,1), *SAT03780
C      1ZC(4,1), PHIXB(1), PHITB(1) *SAT03790
C      2JC(55,1) *SAT03800
C      CCMMCN /IBL1/ MNMAX *SAT03810
C      CCMMCN /IBL2/ N(99), MNINIT AS 'NN' IN SUBRCUTINES FLCAD & EFG *SAT03820
C      CCMMCN /IBL3/ MO, M1, M2, M3 *SAT03830
C      CCMMCN /IBL4/ KMAX, KL, IBCFNL *SAT03840
C      CCMMCN /IBL5/ IBCINL, IBCFNL *SAT03850
C      CCMMCN /IBL6/ KLL *SAT03860
C      CCMMCN /IBL7/ MNMAXC, MAXD(99), MAXS(99), MAXSY(99), IJS(99) *SAT03870
C      CCMMCN /IBL8/ LSTEP, ITR *SAT03880
C      CCMMCN /IBL9/ MAXM *SAT03890
C      CCMMCN /IBL10/ IFREG, NTHMAX *SAT03900
C      CCMMCN /IBL11/ ICORFL, IPASS *SAT03910
C      CCMMCN /IBL12/ KMAX1, KMAX2, NCCNV *SAT03920
C      CCMMCN /IBL13/ ITRMAX, LSMAX *SAT03930
C      CCMMCN /BL1/ A(4,4), BEE(4,4), C(4,4) *SAT03940
C      CCMMCN /BL3/ PR(99), PX(99), PF(99) *SAT03950
C      CCMMCN /BL4/ ZF1M(4,4,99), ZF2M(4,4,99), *SAT03960
C      1 CCMMCN /BL5/ ZF3M(4,4,99), DT(99), DMT(99) *SAT03990
C      CCMMCN /BL6/ MT, APPEARS AS 'EMT' IN SUBRCUTINES INLPOL & FALPOL *SAT04000
C      CCMMCN /BL7/ SOE, CSE, ALOAD *SAT04010
C      CCMMCN /BL8/ DI, S1, GAM(500), DMT(500) *SAT04020
C      CCMMCN /BL9/ R(500), ELIS(4), GEES(4,99) *SAT04030
C      CCMMCN /BL10/ PHIX(99), PHIT(99), PHI(99) *SAT04050
C      CCMMCN /BL11/ DMXI(500), PHEE, TO, T2 *SAT04060
C      CCMMCN /BL12/ TDLI, TDEL *SAT04070
C      CCMMCN /BL13/ OMEGI(4,4), CAPLI(4,4), OMEGL(4,4), CAPLL(4,4), *SAT04080
C      1 CCMMCN /BL14/ UNIT(4,4) *SAT04090
C      CCMMCN /BL15/ LAM2, LSO18, LSCIN *SAT04100
C      CCMMCN /BL16/ NU, UI(99), V1(99), W1(99), V2(99), U2(99), W2(99), U3(99), *SAT04110
C      1 CCMMCN /BL17/ V3(99), W3(99) *SAT04120
C      CCMMCN /BL18/ EPS *SAT04130
C      CCMMCN /BL19/ DEL *SAT04140
C      CCMMCN /BL20/ ELL(4), ELL(4) *SAT04150
C      CCMMCN /BL21/ TH(36) *SAT04160
C      CCMMCN /BL22/ DEOMX(500) *SAT04170
C      CCMMCN /BL23/ JAY(4,4), H(4,4) *SAT04180
C      CCMMCN /BL24/ DL(4,4,99), DG(4,4,99), DF(4,4,99) *SAT04190
C      CCMMCN /BL25/ E(4,4), F(4,4), G(4,4) *SAT04200

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CCMCMCN /BL27/ BX3(99),BT3(99),BX12(99),BE3(55) SAT04210
CCMCMCN /BL28/ EXX3(99),ET13(99),ETX3(99),EX3(99),ET3(99) SAT04220
CCMCMCN /BL29/ BX1(99),BT1(99),BX11(99),BE1(55),BX2(99),BT2(99), SAT04230
1 CCMCMCN /BL30/ BX12(99),BE2(59) SAT04240
1 CCMCMCN /BL30/ EXX1(99),ET11(99),ETX1(99),EX1(99),ET1(99),EXX2(99), SAT04250
CCMCMCN /BL31/ DELSQ,EX11(99) SAT04260
CCMCMCN /BL32/ TKN,ELAST,CHAR,SIGC SAT04270
CCMCMCN /BL100/ TEEO,$DYNMC SAT04280
CCMCMCN /BL101/ DELCAD SAT04290
CCMCMCN /BL102/ MASS(500) SAT04300
CCMCMCN /BL103/ TX(99),TTH(99),TTH(99),MX(99),MTH(99),MXT(99), SAT04310
CCMCMCN /BL110/ QS(59) SAT04320
1 CCMCMCN /BL111/ AB2,ABZ,ABZN,ABZ3,CD2 SAT04330
CCMCMCN /BLPHS/ PHX(99),PHI(99),ICMEGS,ICMEGS,IPSTIF,IOSTIF, SAT04340
CCMCMCN /BLPLOT/ IBBSTF,IBBSTF,IQS,IQS,IMTH,IMSTF,IU,IV,IW,IPFIS, SAT04350
1 CCMCMCN /BLPLT1/ IPHI,IPHI,$PLOIS,$MODAL SAT04360
1 YDECM(200),YBSSTIF(200),YPS(200),YPT(200),YPT(200), SAT04370
2 YDDSTF(200),YPT(200),YPS(200),YPT(200),YPT(200), SAT04380
3 YMT(200),YDT(200),YMT(200),YNS(200),YNTF(200), SAT04390
4 YNSTH(200),YQS(200),YMS(200),YMT(200),YMT(200), SAT04400
5 YU(200),YV(200),XSTATN(200) SAT04410
6 YPHI(200),XSTATN(200) SAT04420
CCMCMCN /BLDATA/ TITILE,NG,IMODE,NCIMEN,IPRINT,LCHMAX,IC SAT04430
CCMCMCN /BLDATA/ TITILE(2),SIGC(2),TITILE(18) SAT04440
CCMCMCN /BLDATA/ TITILE(18) SAT04450
CCMCMCN /BLDATA/ TITILE(18) SAT04460
CCMCMCN /BLDATA/ TITILE(18) SAT04470
CCMCMCN /BLDATA/ TITILE(18) SAT04480
CCMCMCN /BLDATA/ TITILE(18) SAT04490
CCMCMCN /BLDATA/ TITILE(18) SAT04500
CCMCMCN /BLDATA/ TITILE(18) SAT04510
CCMCMCN /BLDATA/ TITILE(18) SAT04520
CCMCMCN /BLDATA/ TITILE(18) SAT04530
CCMCMCN /BLDATA/ TITILE(18) SAT04540
CCMCMCN /BLDATA/ TITILE(18) SAT04550
CCMCMCN /BLDATA/ TITILE(18) SAT04560
CCMCMCN /BLDATA/ TITILE(18) SAT04570
CCMCMCN /BLDATA/ TITILE(18) SAT04580
CCMCMCN /BLDATA/ TITILE(18) SAT04590
CCMCMCN /BLDATA/ TITILE(18) SAT04600
CCMCMCN /BLDATA/ TITILE(18) SAT04610
CCMCMCN /BLDATA/ TITILE(18) SAT04620
CCMCMCN /BLDATA/ TITILE(18) SAT04630
CCMCMCN /BLDATA/ TITILE(18) SAT04640
CCMCMCN /BLDATA/ TITILE(18) SAT04650
CCMCMCN /BLDATA/ TITILE(18) SAT04660
CCMCMCN /BLDATA/ TITILE(18) SAT04670

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SAT04680  
SAT04690  
SAT04700  
SAT04710  
SAT04720  
SAT04730  
SAT04740  
SAT04750  
SAT04760  
SAT04770  
SAT04780  
SAT04790  
SAT04800  
SAT04810  
SAT04820  
SAT04830  
SAT04840

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SAT04980  
SAT04990  
SAT05000  
SAT05010  
SAT05020  
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SAT05070  
SAT05080  
SAT05090  
SAT05100  
SAT05110  
SAT05120  
SAT05130

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99 I=1,4
99 J=1,4
KKLM=J/4+1
KMEGL(I,J)=OMEGL(I,J)*SIGT(KKLM)
CAPLL(I,J)=CAPLL(I,J)*SIGC(KKLM)
LAN=TKN/CHAR
SCE=SIGC/ELAST
C1=1.0-NU
S1=1.0+NU
LAM2=LAM*#2
IF(NDIMEN.LT.1) GC TO 228
ELAST=1.0
TMA=1.0
CHAR=1.0
CC 230 M=1,MAXM
PFT(M)=C.0
PT(M)=0.0
PR(M)=0.0
TI(M)=0.0
NT(M)=0.0
LT(M)=0.0
LMT(M)=C.0
MAXC(M)=0
MAXSY(M)=0
CALL GECM
ICFCK1=IABS(IGAMMA)+IABS(IOMEGS)+IABS(IOMEGT)+IABS(ICEOMS)
+IABS(IRADII)
ICFCK2=IABS(IBSTIF)+IABS(IDSTIF)+IABS(IBBSTF)+IABS(ICDSTF)
IF (.NOT. $PLOTS) GC TO 1001
CC 2 K=1,KMAX
XSTATN(K)=FLOAT(K)
IF (ICFCK1.EQ.0) GO TO 1001
CC 1 K=1,KMAX
XRADII(K)=R(K)*CHAR
YGAMMA(K)=GAM(K)/CHAR
YCEMG(K)=CMXI(K)/CHAR
YCEMG(K)=GMT(K)/CHAR
YCECMS(K)=DEOMX(K)/(CHAR*CHAR)
CCNTINUE
1001 CCNTINUE
CC 86 K=1,KMAX
86 MASS(K)=0.

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```

WRITE(6,802)
CC 578 K=1,KMAX
RKK=R(K)*CHAR
CMXIK=CMXI(K)/CHAR
GAMK=GAM(K)/CHAR
CMTK=CMT(K)/CHAR
CECMXK=CECMX(K)/(CHAR*CHAR)
WRITE(6,803) K,RKK,GAMK,CMXIK,OMTK,DEOMXK
NC=C
NJ=0
NJ2=C
NJ3=C
AEN=CHAR/SIGO/TKN
ZN=SIGO*TKN
WRITE(6,112)
CC 88 K=1,KMAX
CALL BCE(K,B,DB,D,CC)
EST=ELAST*TKN
ZST=ELAST*TKN**3
B=B*BST
CC=C*ZST
CB=CB/CHAR*BST
LC=CC/CHAR*ZST
WRITE(6,71) K,B,D,CB,DD
YESIF(K)=B
YESSTIF(K)=C
YESSTIF(K)=CB
YESSTIF(K)=CD
CCNTINLE
CALL PLCCAD(1,Z)
CALL TLCCAD(1,Z)
CC 885 N=1,MNMAX
WRITE(6,113) N(M)
WRITE(6,114)
ICHECK3=IABS(IPR)+IABS(IPS)+IABS(IPT)+IABS(ITT)+IABS(IMT)
+IABS(IDTT)+IABS(IDMT)
1
DC 890 K=1,KMAX
CALL PLCCAD(K,Z)
CALL TLCCAD(K,Z)
PPN=PT(M)/ABN
PTM=PT(M)/ABN
PTM=PT(M)/ABN
PTM=TT(M)*ZN
PTM=MT(M)/CHAR*ZN
CMTM=DMT(M)*ZN*TKN/(CHAR*CHAR)
WRITE(6,115) K,PRM,PTM,TTM,EMTM,DTM,CMTM

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SAT0611CO
SAT061110
SAT061120
SAT061130
SAT061140
SAT061150
SAT061160
SAT061170
SAT061180
SAT061190
SAT061200
SAT062110
SAT062220
SAT062230
SAT062240
SAT062250
SAT062260
SAT062270
SAT062280
SAT062290
SAT063000
SAT063110
SAT063320
SAT063330
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SAT063380
SAT063390
SAT064000
SAT064110
SAT064220
SAT064230
SAT064440
SAT064450
SAT064460
SAT064470
SAT064480
SAT064490
SAT064500
SAT065110
SAT065120
SAT065230
SAT065330
SAT065540
SAT065550
SAT065560
SAT065570

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F I=IPRINT  
F L I=LSTEP/IFPRINT  
F L I=L I  
F F T=F L I -FL/FI CALL PHITB)  
1 IF(FI,EC.O.)  
IF(JD,PP,XC.1) ITRPR=1  
IF(LSTEP.EQ.1) ITRPR=1  
IF(I,STEP.GE.LSMAX) ITRPR=1  
IF(LSTEP.GE.LSMAX) GO TO 360  
CC CC 61 MN=1,MNMAX  
CC CC 61 K=1,KMAX2  
IK=K+(MN-1)\*KMAX2  
ZNA=2.0+Z(I,IK)-ZO(I,IK)  
ZC(I,IK)=Z(I,IK)  
Z(I,IK)=ZN  
1 Z(I,IK)=LSTEP.GE.LSMAX GO TO 360  
ALCAC=ALOAD+DELOAD  
LSTEP=LSTEP+1  
ITR=1  
GO TO 400  
WRITE(6,221) NO  
WC TO 500  
ITR=ITR+1  
GO TO 400  
IF(LSTEP-1) 310,310,320  
WRITE(6,223)  
WC TO 500  
WRITE(6,222)  
LCFANG=LCHANG+1  
LSTEP=LSTEP-1  
ALCAC=ALOAD-DELOAD  
CC CC 32 MA=1,MNMAX  
CC CC 32 K=1,KMAX2  
IK=K+(MN-1)\*KMAX2  
QC CC 32 I=1,4  
Z(I,IK)=ZC(I,IK)  
GC TO 62  
\*\*\*\*\*  
71 FCRMAT(20X,13,4X,4E20.6)  
112 FCRMAT(///17X,12H STIFFNESS 20H B STIFFNESS 20H D STIFFNESS 20H PRIME  
112 IFFNESS 20H  
112 FCRMAT(///25X,44H PRESSURE AND TEMPERATURE COEFFICIENTS FOR N=13,8H  
1 FLOW//)  
114 FCRMAT(5X,7H STATION,3X,15H PR 15H MT 15H PX 15H DTT 15H  
1 PT



CCMMCN	/BL5/	TT(99), MT(99), DT(99), DMT(99)	SAT07060
CCMMCN	/BL6/	MT, APPEARS AS 'EMT' IN SUBROUTINES INLPC & FALPOL	SAT07070
CCMMCN	/BL7/	SOE, CSE, ALOAD	SAT07080
CCMMCN	/BL8/	DI, SI	SAT07090
CCMMCN	/BL9/	R(500), GAM(500), DMT(500)	SAT07100
CCMMCN	/BL10/	FFS(4,99), ELIS(4), CEES(4,99)	SAT07120
CCMMCN	/BL11/	PHIX(99), PHIT(99), FTI(99)	SAT07130
CCMMCN	/BL12/	OMXI(500), PHEE, IO, I2	SAT07140
CCMMCN	/BL13/	TDLI, TDEL	SAT07150
1	CCMMCN	OMEGI(4,4), CAPLI(4,4), OMEGL(4,4), CAPLL(4,4),	SAT07160
1	CCMMCN	UNIT(4,4)	SAT07170
1	CCMMCN	LAM2, LSD18, LSCIN	SAT07180
1	CCMMCN	NU, UI(99), V1(99), W1(99), V2(99), L2(99), W2(99), U3(99),	SAT07190
1	CCMMCN	V3(99), W3(99)	SAT07200
1	CCMMCN	EPS	SAT07210
1	CCMMCN	DEL	SAT07220
1	CCMMCN	ELI(4), ELL(4)	SAT07230
1	CCMMCN	TH(36)	SAT07240
1	CCMMCN	DEOMX(500)	SAT07250
1	CCMMCN	JAY(4,4), F(4,4), DG(4,4,99), DF(4,4,99)	SAT07270
1	CCMMCN	DL(4,4,99), G(4,4)	SAT07280
1	CCMMCN	EX(4,99), BT3(99), BX12(99), BE2(99)	SAT07290
1	CCMMCN	EXX3(99), ETI3(99), ETX3(99), EX3(99), ET3(99)	SAT07300
1	CCMMCN	EXX1(99), ETI1(99), BXTI1(99), BE1(99), BX2(99), BT2(99),	SAT07310
1	CCMMCN	BXT2(99), BE2(99)	SAT07320
1	CCMMCN	EXX1(99), ETI1(99), ETX1(99), ET1(99), EXX2(99),	SAT07330
1	CCMMCN	ETI2(99), ETX2(99), EX2(99), ET2(99)	SAT07340
1	CCMMCN	DELSD, EXTI(99)	SAT07350
1	CCMMCN	TKN, ELAST, CHAR, SIGC	SAT07360
1	CCMMCN	TEEG, \$DYNMC	SAT07370
1	CCMMCN	DELSD	SAT07380
1	CCMMCN	DELOAD	SAT07390
1	CCMMCN	MASS(500)	SAT07400
1	CCMMCN	TX(99), TTH(99), TXT(99), MX(99), MTH(99), MXT(99),	SAT07410
1	CCMMCN	QS(99)	SAT07420
1	CCMMCN	ABZ, ABZ0, ABZN, ABZ3, DC2	SAT07430
1	CCMMCN	PHX(99), PHT(99)	SAT07440
1	CCMMCN	IRADII, IGAMMA, ICMES, IOMEGT, IDEOMS, IPSTIF, IDSTIF,	SAT07450
1	CCMMCN	IBBSTF, IDSTF, IPR, IPS, IPT, IIT, IMT, ICTT, ICMT, IAS,	SAT07460
1	CCMMCN	INTH, INSTH, IQS, IMS, IMTH, INSTH, IU, IV, IW, IFHIS,	SAT07470
1	CCMMCN	IPHT, IPHI, \$PLOTS, \$MODAL	SAT07480
1	CCMMCN	XRADII(200), YGAMMA(200), YCMEGS(200), YCMEGT(200),	SAT07490
1	CCMMCN	YRDECMS(200), YBSTIF(200), YPS(200), YPT(200), YTT(200),	SAT07500
1	CCMMCN	YDOSTF(200), YPR(200), YDMT(200), YNS(200), YNTH(200),	SAT07510
1	CCMMCN	YMT(200), YDT(200), YQS(200), YMS(200), YMTH(200), YMSTH(200),	SAT07520
1	CCMMCN	YNSTH(200), YV(200), YW(200), YPHIS(200), YPHIT(200),	



SAT07990  
SAT08000  
SAT08010  
SAT08020  
SAT08030  
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SAT08370  
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SAT08390  
SAT08400  
SAT08410  
SAT08420  
SAT08430  
SAT08440  
SAT08450  
SAT08460

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LT(M)=0.0
DMT(M)=C.0
MAXLC(M)=0
MAXSS(M)=0
MAXSY(M)=0
CALL GECM
1 ICFCK1=IABS((IGAMMA)+IABS(IOMEGS))+IABS(IOMEGT))+IABS(ICEOMS)
  + IABS(IRADI)
  ICFCK2=IABS(IBSTIF)+IABS(IDSTIF)+IABS(IBBSTF)+IABS(IDDSTF)
  IF (.NOT. $PLOTS) GO TO 1001
  CC 2 K=1,KMAX
2 XSTATN(K)=FLQAT(K)
  IF (ICHECK1.EQ.0) GO TO 1001
  CC 1 K=1,KMAX
  XRADII(K)=R(K)*CHAR
  YGAMMA(K)=GAM(K)/CHAR
  YCMEGS(K)=OMXI(K)/CHAR
  YCEMGST(K)=CMT(K)/CHAR
  YCECMS(K)=DEOMX(K)/(CHAR*CHAR)
  CC CONTINUE
1001 CC CONTINUE
  CC 1 K=1,KMAX
  TEED=1.0
  IF (ADIMEN.EQ.1) TEED=1.0
  CC 579 K=1,KMAX
  RKK=R(K)*CHAR
  CMXIK=CMXI(K)/CHAR
  GAMK=GAM(K)/CHAR
  CMTK=CMT(K)/CHAR
  DECMXK=DEOMX(K)/(CHAR*CHAR)
  ANSS=MASS(K)*TEED**2*ELAST*TKN/CHAR**2
  WRITE(6,813) K,RKK,GAMK,CMXIK,CMTK,DEOMXK,ANSS
979 NC=C
80E M1=0
  M2=0
  M3=0
  AEN=CHAR/SIGO/TKN
  ZN=SIGC*TKN
  WRITE(6,112)
  CC 888 K=1,KMAX
  CALL BDE(K,B,DB,D,CC)
  BST=ELAST*TKN
  ZST=ELAST*TKN**3
  B=B*BST
  C=C*ZST
  CB=CB/CHAR*BST
  CC=DD/CHAR*ZST
  WRITE(6,71) K,B,C,CB,DD

```



```

83C      TM=ACD*ZDOT(3,MK)
834      TM=AMD*ZDOT(4,MK)
      KK=K-1
      WRITE(6,71) KK,TU,TV,TH,TM
      CC=830
      I=1,4
      Z(I,MK)=Z(I,MK)+ZCCT(I,MK)*DELCAC
      Z2(I,MK)=ZC(I,MK)-ZDOT(I,MK)*DELCAC
      Z3(I,MK)=ZC(I,MK)-2.*ZDOT(I,MK)*CELOAD
      CCNTINUE
      ALCAD=1.0
      CALL IMPERF (PHIXE,PHITB)
      CALL FMAXTRX (P,X,ZC,Z2,Z3,DEE,DST)
      LSTEP=1
      LCHANG=C
      ITR=1
      ICCRFL=0
      IF(MNMAX.EQ.MAXM) ICORFL=1
      IPASS=0
      ITTEST=0
      CALL XANDZ (P,DEE,DST,X,Z,ZC,Z2,Z3,ZDOT,IS,JS,IC,JD,PTIXB,PHITB)
      IF(ITRMAX.EQ.1) GO TO 5C
      MNMAXC=MNMAX
      IF(IPASS.LT.2) CALL MODES (IS,JS,IC,JD,P,X,ZC,Z2,Z3,CEE,CST)
      IF(NCCNV.EQ.1) GO TO 5D
      IF(ITR.LT.ITRMAX) GC TO 23
      GC TO 365
5C      FL=LSTEP
      FI=IPRINT
      LI=LSTEP/IPRINT
      FLI=LI
      FT=FLI-FL/FI
      IF(FT.EQ.0.) CALL (PHIXB,PHITB)
      ILL(JD,PTIXB,PHITB)
      IF(LSTEP.GE.LSMAX) GC TC 360
      CC=65
      MN=1,MNMAX2
      DC=65
      K=1,KMAX2
      IK=K+(MN-1)*KMAX2
      DC=65
      I=1,4
      ZN=3.0*(Z(I,I)-ZC(I,IK))+Z2(I,IK)
      Z2(I,IK)=Z2(I,IK)
      Z3(I,IK)=Z3(I,IK)
      ZC(I,IK)=ZN
      ALCAD=1.0
      LSTEP=LSTEP+1
      ITR=1
      GC TO 400
      ITR=ITR+1
      23

```

SAT089550  
 SAT08960  
 SAT08970  
 SAT08980  
 SAT08990  
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 SAT09370  
 SAT09380  
 SAT09390  
 SAT09400  
 SAT09410  
 SAT09420  
 SAT09430  
 SAT09440







```

C *** FIND MAX & MIN FOR SCALE COMPUTATIONS *** SAT109930
C *** XMAX=-1.E20 *** SAT109940
C *** XMIN=1.E20 *** SAT109950
C *** YMAX=-1.E20 *** SAT109960
C *** YMIN=1.E20 *** SAT109970
C *** DO 1 I=1,KN *** SAT109980
C *** IF(X(I).LT.XMAX) GO TO 6 *** SAT109990
C *** IF(X(I).GT.XMIN) GC TO 7 *** SAT110000
C *** IF(Y(I).LT.YMAX) GC TO 8 *** SAT110010
C *** IF(Y(I).GT.YMIN) GC TO 1 *** SAT110020
C *** 1 CCNTINUE *** SAT110030
C *** IF NOT AUTOSCALE GC TC CALL DRAWIT *** SAT110040
C *** IF(N.GT.0) GO TO 5 *** SAT110050
C *** COMPUTE X-SCALE & NEW XMAX AND XMIN *** SAT110060
C *** CALL SCALIT(XMAX,XMIN,4) *** SAT110070
C *** COMPUTE Y-SCALE & NEW YMAX AND YMIN *** SAT110080
C *** CALL SCALIT(YMAX,YMIN,6) *** SAT110090
C *** PLCT CURVE *** SAT110100
C *** 5 CALL DRAWIT(X,Y,KN,RANGE,1,MDCUR) *** SAT110110
C *** IF(MDCUR.EQ.1.CR.MDCUR.EC.2) RETURN *** SAT110120
C *** PRINT SCALES WHEN LAST CURVE PLCTED *** SAT110130
C *** XS=(XMAX-XMIN)/80. *** SAT110140
C *** YS=(YMAX-YMIN)/60. *** SAT110150
C *** 100 WRTTE(6,100) XS,YS *** SAT110160
C *** 100 FCRMAT(15X,'X-SCALE: "X"=,E10.3," UNITS"/ *** SAT110170
C *** 1 RETURN *** SAT110180
C *** ENCL *** SAT110190
C *** SLERQUITINE SCALIT(XMAX,XMIN,IDIV) *** SAT110200
C *** CIV=IDIV *** SAT110210
C *** *** SAT110220
C *** *** SAT110230
C *** *** SAT110240
C *** *** SAT110250
C *** *** SAT110260
C *** *** SAT110270
C *** *** SAT110280
C *** *** SAT110290
C *** *** SAT110300
C *** *** SAT110310
C *** *** SAT110320
C *** *** SAT110330
C *** *** SAT110340
C *** *** SAT110350
C *** *** SAT110360
C *** *** SAT110370
C *** *** SAT110380
C *** *** SAT110390
C *** *** SAT110400

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C*****
C***** RCUND MAXIMUM TO NEXT HIGHEST 2 SIG FIGS *****
C***** XMAX=AMAXI(0.,XMAX)
C***** CALL RCUND(XMAX,IMX,FMX)
C***** IMX=IMX-1
C***** FMX=FMX*10.
C***** 3 XMAX=FMX*10.
C***** IF(XMAX.GE.XMAX) GC TO 2
C***** FMX=FMX
C***** IMX=IMX
C***** GC TO 3
C***** RCUND MINIMUM TO NEXT LOWEST 2 SIG FIGS *****
C***** XMIN=AMINI(0.,XMIN)
C***** CALL RCUND(XMIN,IMN,FMN)
C***** IMN=IMN-1
C***** FMN=FMN*10.
C***** 14 XMIN=FMN*10.
C***** IF(XMIN.GE.XMIN) GC TO 11
C***** FMN=FMN
C***** IMN=IMN
C***** GC TO 14
C***** RCUND MAX & MIN TC 1. OR .1 IF RANGE LARGE *****
C***** 11 XSC=XPX-XMN
C***** IM=1
C***** 5 IF(XSC/CIV.LE.SM) GC TO 12
C***** IF(ABS(XMN).LT.SM.AND.ABS(XMN).GT.0.) XMN=SIGN(SM,XMN)
C***** IF(ABS(XMX).LT.SM.AND.ABS(XMX).GT.0.) XMX=SIGN(SM,XMX)
C***** 12 IF(IM.GT.0) GO TO 19
C***** SM=1
C***** IM=IM+1
C***** GC TO 9
C***** RCUND RANGE (MAX-MIN) TC 2 SIG FIGS *****
C***** 15 XSC=XMX-XMN
C***** CALL RCUND(XSC,ISIC,FACTX)
C***** FINE FACTOR WHICH IS MULTIPLE OF IDIV *****
C***** FACTX=FACTX*10.
C***** CFAC=FACTX
C*****
SAT110410
SAT110420
SAT110430
SAT110440
SAT110450
SAT110460
SAT110470
SAT110480
SAT110490
SAT110500
SAT110510
SAT110520
SAT110530
SAT110540
SAT110550
SAT110560
SAT110570
SAT110580
SAT110590
SAT110600
SAT110610
SAT110620
SAT110630
SAT110640
SAT110650
SAT110660
SAT110670
SAT110680
SAT110690
SAT110700
SAT110710
SAT110720
SAT110730
SAT110740
SAT110750
SAT110760
SAT110770
SAT110780
SAT110790
SAT110800
SAT110810
SAT110820
SAT110830
SAT110840
SAT110850
SAT110860
SAT110870
SAT110880

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1C CCNT INUE
E FACT=FACT*10.**(-IDD)
IS=IS+IDD
C ***
C *** RCLND MANTISSA TO 2 SIG FIGS
C ***
C *** IFAC=FACT*10.+*05
C ***
C *** FACT=IFAC
C ***
C *** IF(FACT.LT.10.) GC TO 20
C ***
C *** SET TO 1 IF LESS THAN 10.
C ***
C *** FACT=1.
C ***
C *** IS=IS+1
C ***
C *** IF INPUT NEGATIVE, SET MANTISSA NEGATIVE
C ***
C *** 2C IF(ANUM.LT.0.) FACT=-FACT
C ***
C *** RETURN
C ***
C *** SET TO C. IF 0.
C ***
C *** IS=IS+1
C ***
C *** FACT=0.
C ***
C *** IS=C
C ***
C *** RETURN
C ***
C *** SUBROUTINE GRID(X,Y,NCATA,RANGE,KKZ,MODCUR)
C ***
C *** DIMENSION X(1),Y(1),XSCALE(5),YSCALE(7)
C ***
C *** INTEGER I2,GRID,BLANK,DCT,XCHAR(4)/1H+,1H-,1H*,1Hx/
C ***
C *** NCATA=NCAT,TA*KKZ
C ***
C *** IF(MODCUR.GT.1) GC TO 444
C ***
C *** GRID IS THE MATRIX USED TO PLOT THE POINTS
C ***
C *** IERR=0
C ***
C *** XMAX=RANGE(1)
C *** XMIN=RANGE(2)
C *** YMAX=RANGE(3)
C *** YMIN=RANGE(4)
C ***
C *** CHECKING X AND Y PCINTS AND PLOTTING THOSE CUT OF RANGE
C *** AT THE MARGIN
C ***
C *** DC 30 I=1,KCATA,KKZ

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SAT1111370
SAT111380
SAT111390
SAT111400
SAT111410
SAT111420
SAT111430
SAT111440
SAT111450
SAT111460
SAT111470
SAT111480
SAT111490
SAT111500
SAT111510
SAT111520
SAT111530
SAT111540
SAT111550
SAT111560
SAT111570
SAT111580
SAT111590
SAT111600
SAT111610
SAT111620
SAT111630
SAT111640
SAT111650
SAT111660
SAT111670
SAT111680
SAT111690
SAT111700
SAT111710
SAT111720
SAT111730
SAT111740
SAT111750
SAT111760
SAT111770
SAT111780
SAT111790
SAT111800
SAT111810
SAT111820
SAT111830
SAT111840

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UUUUUUUUUUUUUUUUUUUUUUUUUUUUUU





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1 2 3 4 5 6
C**
DIMENSION PTF(500), PF(500), XSTATN(200), YPHI(200), YV(200), YW(200), YPFI(200),
AEZC=SIGO/ELAST
IF ($DYNMC) GO TO 181
WRITE(6,101) LSTEP,ALOAD,ITR
CC TO 182
TI=LSTEP*DELOAD
CTI=TI*TEEG
WRITE(6,151) LSTEP,TI,DTI,ITR
LAN=TKN/CHAR
ENL=1
AEZ=SIGC*TKN
AEZ3=ABZ*TKN*TKN/CHAR
AEZN=CHAR*SIGO/ELAST
IF (ITRMAX.EQ.1) ENL=0.
CC2=1.-NU*#2
CC1=1./CD2
CPI=1./SI
CNI=1./CI
ICLSQI=5/CELSQ
ICCHK1=IABS(INSTH)+IABS(INSTH)+IABS(IQS)+IABS(IMS)
1 ICCHK2=IABS(IU)+IABS(IV)+IABS(IW)+IABS(IPHIS)+IABS(IPHIT)
1 IF (NT+MAX.EQ.0) GO TO 991
CC 21 NTH=1,NTHMAX
CC 1 MN=1,MNMAX
I1=1+(MN-1)*KMAX2
I2=I1+1
U1(MN)=Z(1,I1)
U2(MN)=Z(1,I2)
V1(MN)=Z(2,I1)
V2(MN)=Z(2,I2)
W1(MN)=Z(3,I1)
W2(MN)=Z(3,I2)
1 WDET=TF(ATF) THET
WRITE(6,116) THET
CC 121 K=1,KMAX
K1=K+1
CALL BCB(K,BS,DB,CS,DD)
IF (K.EQ.1.AND.IBCINL.LT.0) CALL PCLE(K,P,DEE,CST,X,Z,ZO,Z2,Z3,
1 ZCCT,IS,JS,JD,PHIXB,PHITE)
YDEGMS(200),YBSTIF(200),YDSTIF(200),YBSTF(200),YBSTF(200),
YDDSTF(200),YPR(200),YPS(200),YPT(200),YPT(200),
YMT(200),YDIT(200),YDMT(200),YNS(200),YNTF(200),
YNSTH(200),YQS(200),YMS(200),YMT(200),YMT(200),
YU(200),YV(200),YW(200),YPFI(200),YPFI(200),
YPHI(200),XSTATN(200)
SAT13770
SAT13780
SAT13790
SAT13800
SAT13810
SAT13820
SAT13830
SAT13840
SAT13850
SAT13860
SAT13870
SAT13880
SAT13890
SAT13900
SAT13910
SAT13920
SAT13930
SAT13940
SAT13950
SAT13960
SAT13970
SAT13980
SAT13990
SAT14000
SAT14010
SAT14020
SAT14030
SAT14040
SAT14050
SAT14060
SAT14070
SAT14080
SAT14090
SAT14100
SAT14110
SAT14120
SAT14130
SAT14140
SAT14150
SAT14160
SAT14170
SAT14180
SAT14190
SAT14200
SAT14210
SAT14220
SAT14230
SAT14240

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IF(K-EQ.1-AND.1BCINL.LT.0) GO TC 999
IF(K-EQ.KMAX-AND.1BCFNL.LT.0) CALL POLE(K,P,CEE,DST,X,Z,ZO,Z2,Z3,
1 ZCCT,IS,JS,JD,PHIXB,PHITB)
IF(K-EQ.KMAX-AND.1BCFNL.LT.0) GO TO 999
CALL PHIBET(K,Z,IS,JS,JD,PHIXB,PHITB)
CEX=DEGMX(K)
FRA=1./R(K)
CX=CMXI(K)
CT=CMT(K)
GA=GAK(K)
DCXT=GX-CT
CCC=GA*COXT
CC2C=CC2*DS
CC 3 MN=1,MNMAX3
ENR=EN*FRA
CALL TLOAD(K,Z)
TTS=TT(MN)*ALOAD
EX=(U3(MN)-U1(MN))*TDLI+OX*W2(MN)+ENL*OSE*(EX3(MN)+BE3(MN))
ET=ENR*V2(MN)+GA*U2(MN)+OT*W2(MN)+ENL*OSE*(ET3(MN)+BE3(MN))
EXT=.5*((V3(MN)-V1(MN))*TDLI-ENR*U2(MN)-GA*V2(MN)+ENL*SCE*BXT3(MN))
1
KT=ENR*PHIT(MN)+GA*PHIX(MN)
KXT=.5*(ENR*(-PHIX(MN)-GA*W2(MN)+(W3(MN)-W1(MN))*TDLI)+GCO*V2(MN)
+OT*(V3(MN)-U1(MN))*TDLI-GA*PHIT(MN)-CCXT*PHI(MN))
1
TX(MN)=ES*(EX+NU*ET)-ITS
TTH(MN)=BS*(ET+NU*EX)-ITS
XT(MN)=BS*DI*EXT
MKI=K1+(MN-1)*KMAX2
MX(MN)=Z(4,MKI)
MTF(MN)=NU*MX(MN)+DD20*KT-D1*MT(MN)*ALOAD
XT(MN)=DS*DI*KXT
MKI=MKI+1
MKKI=MKI-1
CS(MN)=SIGO*TKN*LAM2*(GA*MX(MN)+(Z(4,MKI)-Z(4,MKKI))*TDLI
+ENR*MX(MN)-GA*PHI(MN))
1
MX(MN)=MX(MN)*ABZ3
MTF(MN)=MT(MN)*ABZ3
XT(MN)=XT(MN)*ABZ3
TX(MN)=TX(MN)*ABZ
TTH(MN)=TTH(MN)*ABZ
TTH(MN)=TTH(MN)*ABZ
PHIX(MN)=PHIX(MN)*ABZ
PHIT(MN)=PHIT(MN)*ABZC
PHI(MN)=PHI(MN)*ABZ
L1(MN)=L2(MN)
L2(MN)=L3(MN)
V1(MN)=V2(MN)

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SAT114250  
SAT114260  
SAT114270  
SAT114280  
SAT114290  
SAT114300  
SAT114310  
SAT114320  
SAT114330  
SAT114340  
SAT114350  
SAT114360  
SAT114370  
SAT114380  
SAT114390  
SAT114400  
SAT114410  
SAT114420  
SAT114430  
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SAT114460  
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SAT114480  
SAT114490  
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SAT114680  
SAT114690  
SAT114700  
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 SAT114970  
 SAT114980  
 SAT114990  
 SAT115000  
 SAT115010  
 SAT115020  
 SAT115030  
 SAT115040  
 SAT115050  
 SAT115060  
 SAT115070  
 SAT115080  
 SAT115090  
 SAT115100  
 SAT115110  
 SAT115120  
 SAT115130  
 SAT115140  
 SAT115150  
 SAT115160  
 SAT115170  
 SAT115180  
 SAT115190  
 SAT115200

```

3  V1(MN)=V3(MN)
   W2(MN)=W3(MN)
   FIFREQ=IFREQ
   FKTEST=FKTEST/IFREQ
   IF(K.EQ.1.OR.K.EQ.KMAX) GO TO 2
   X(1,K)=0.
   X(2,K)=C.
   X(3,K)=C.
   X(4,K)=C.
   PTF(K)=0.
   AMX=0.
   AMTH=0.
   ANX=0.
   ANTH=0.
   ANXTH=0.
   ACS=0.
   IF(JUMP.EQ.2) GO TO 73
   IF(72 MN=1,MNMAXO
   EN=N*TFET
   CS=SIN(FC)
   CS=CS*(FC)
   X(1,K)=X(1,K)+U1(MN)*CS*ABZN
   X(2,K)=X(2,K)+V1(MN)*SN*ABZN
   X(3,K)=X(3,K)+W1(MN)*CS*ABZN
   X(4,K)=X(4,K)+PHIX(MN)*CS
   PTF(K)=PTF(K)+PHIT(MN)*SN
   AMX=AMX+MX(MN)*CS
   AMTH=AMTH+MTH(MN)*CS
   ANXTH=ANXTH+MX(MN)*SN
   ANX=ANX+TX(MN)*CS
   ANTH=ANTH+TTH(MN)*CS
   ACS=ACS+QS(MN)*CS
   ANXTH=ANXTH+TX(MN)*SN
   PTF(K)=PTF(K)+PHI(MN)*SN
   C*****
72 GC TO 425
   CC 14 MN=3,MNMAXO,JUMP
73 EN=N*TFET
   SN=SIN(FC)

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```

661 IF(K.EQ.1.OR.K.EQ.KMAX) GO TO 661
IF(PKTEST.NE.0.) GO TO 658
IF(K.EQ.1) WRITE(6,217)
WRITE(6,218) K,X(1,K),X(2,K),X(3,K),X(4,K),FTF(K),PF(K)
IF ($MODCAL.OR.(ICFCK2.EQ.0)) GO TO 658
YL(K)=X(1,K)
YV(K)=X(2,K)
YK(K)=X(3,K)
YPHIS(K)=X(4,K)
YPHIT(K)=PF(K)
YFPI(K)=PF(K)
DC 659 I=1,4
DO 659 X(I,K)=0.
CCNTINUE
658 IF ($PLCTTS.AND..NOT.$MOCAL.AND.((ICCHK1.GT.0).OR.(ICFCK2.GT.0)))
659 CCNTINUE
660 IF CALL PLOT2(NTH)
21 CCNTINUE
551 IF(IMCODE.LE.0) RETURN
CC 534 MN=1,MNMAXO
WRITE(6,749) N(MN)
DC 521 MM=1,MNMAXC
I1=1+(MM-1)*KMAX2
I2=I1+1
U1(MM)=Z(1,I1)
U2(MM)=Z(1,I2)
V1(MM)=Z(2,I1)
V2(MM)=Z(2,I2)
W1(MM)=Z(3,I1)
W2(MM)=Z(3,I2)
CCNTINUE
521 DC 445 K=1, KMAX
KI=K+1
CALL BCB(K,BS,DB,CS,DC)
IF(K.EQ.1.AND.IBCINL.LT.0) CALL FCLE(K,P,DEE,CST,X,Z,ZO,Z2,Z3,
17CCT,IS,JS,IO,JD,PHIXB,PHITB)
IF(K.EQ.KMAX.AND.IBCFNL.LT.0) CALL POLE(K,P,DEE,DST,X,Z,ZO,Z2,Z3,
17CCT,IS,JS,IO,JD,PHIXB,PHITB)
TXZ=TX(MN)
THZ=TH(MN)
TXZ=TX(MN)
THZ=TH(MN)
ANXZ=MX(MN)
ANTH=MT(MN)
ANXZ=MX(MN)
ANTH=MT(MN)
CSZ=QS(MN)
X(1,K)=PHIX(MN)
X(2,K)=PHIT(MN)
X(3,K)=PHI(MN)
IF(K.EQ.1.AND.IBCINL.LT.0) GO TO 583

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SAT115690
SAT115700
SAT115710
SAT115720
SAT115730
SAT115740
SAT115750
SAT115760
SAT115770
SAT115780
SAT115790
SAT115800
SAT115810
SAT115820
SAT115830
SAT115840
SAT115850
SAT115860
SAT115870
SAT115880
SAT115890
SAT115900
SAT115910
SAT115920
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SAT115950
SAT115960
SAT115970
SAT115980
SAT115990
SAT116000
SAT116010
SAT116020
SAT116030
SAT116040
SAT116050
SAT116060
SAT116070
SAT116080
SAT116090
SAT116100
SAT116110
SAT116120
SAT116130
SAT116140
SAT116150
SAT116160

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```

IF(K.EQ.KMAX.AND.IBCFNL.LT.O) GC TC 583
CALL PHIBET(K,Z,IS,JS,IO,JD,PHIXB,PHITB)
LEX=DECMX(K)
FRA=1./R(K)
CX=CMXI(K)
CT=CTI(K)
GA=GAM(K)
CCXT=OX-CT
GCC=GA*CCXT
CC2C=CC2*DS
ENR=EN(MN)
ENR=EN*RRRA
CALL TLCCAD(K,Z)
TTS=TT(MN)*ALOAD
EX=(U3(MN)-U1(MN))*TTS
ET=ENR*V2(MN)+GA*U2(MN)+OT*W2(MN)+ENL*OSE*(BX3(MN)+BE3(MN))
EXT=.5*((V3(MN)-V1(MN))*TDLI-ENR*U2(MN)-GA*V2(MN)+ENL*SOE*BXT3(MN))
1)
KT=ENR*PHIT(MN)+GA*PHIX(MN)
KXT=.5*(ENR*(-PHIX(MN)-GA*W2(MN)+(W3(MN)-W1(MN))*TDLI)+GCO*V2(MN)
+OT*(V3(MN)-V1(MN))*TDLI-GA*PHIT(MN)-CCXT*PHI(MN))
1)
TXZ=(BS*(EX+NU*ET)-TTS)*ABZ
THZ=(BS*(ET+NU*EX)-TTS)*ABZ
TXIZ=BS*DI*EXT*ABZ
MXI=KI+(MN-1)*KMAX2
AMXZ=Z(4,MKI)
AMTHZ=NU*AMXZ+DD2D*KT-D1*MT(MN)*ALCAD
AMXIZ=CS*CI*KXT
MKI1=MKI+1
MKK1=MKI-1
CS2=SIGO*TKN*LAM2*(GA*AMXZ+(Z(4,MKI1)-Z(4,MKI1))*TCLI+ENR*AMXIZ
-GA*AMTHZ)
1)
AMXZ=AMXZ*ABZ3
AMTHZ=AMTHZ*ABZ3
AMXIZ=AMXIZ*ABZ3
X(1,K)=PHIX(MN)*ABZG
X(2,K)=PHIT(MN)*ABZC
X(3,K)=PHI(MN)*ABZC
CL1(MN)=L2(MN)
CL2(MN)=L3(MN)
V1(MN)=U3(MN)
V2(MN)=V3(MN)
W1(MN)=W2(MN)
W2(MN)=W3(MN)
FK=K-1
FFREQ=IFREQ
KTST=(K-1)/IFREQ

```

SATI1617C  
SATI16180  
SATI16190  
SATI16200  
SATI16210  
SATI16220  
SATI16230  
SATI16240  
SATI16250  
SATI16260  
SATI1627C  
SATI16280  
SATI16290  
SATI16300  
SATI16310  
SATI16320  
SATI16330  
SATI16340  
SATI16350  
SATI16360  
SATI16370  
SATI16380  
SATI16390  
SATI16400  
SATI16410  
SATI16420  
SATI16430  
SATI16440  
SATI16450  
SATI16460  
SATI16470  
SATI16480  
SATI16490  
SATI16500  
SATI16510  
SATI16520  
SATI16530  
SATI16540  
SATI16550  
SATI16560  
SATI16570  
SATI16580  
SATI16590  
SATI16600  
SATI16610  
SATI16620  
SATI16630  
SATI16640

```

543 FKIST=FKTST
544 IF(K.EQ.1) FIFREQ=FKTST
545 IF(FKTEST.NE.0.) GC TO 445
546 CCNTINUE
547 IF(K.EQ.1) WRITE(6,117)
548 WRITE(6,118) K, TXZ, TTHZ, TXTZ, QSZ, AMXZ, AMTHZ, AMXTZ
549 IF(.NOT.$PLOTS.OR..NOT.$MODAL.EC.0) GC TO 445
550 YNTH(K)=TXZ
551 YNSTH(K)=TTHZ
552 YCS(K)=CSZ
553 YNTH(K)=AMXZ
554 YNSTH(K)=AMTHZ
555 CCNTINUE
556 WRITE(6,217)
557 DC 447 K=1, KMAX
558 FK=K-1
559 FIFREQ=1
560 KIST=(K-1)/FIFREQ
561 FKIST=KIST
562 FKTEST=FK/FIFREQ-FKTST
563 IF(K.EQ.1) CR.K.EQ.KMAX) GO TO 593
564 IF(FKTEST.NE.0.) GO TO 447
565 KZ=K+1+(MN-1)*KMAX2
566 LF=Z(1,KZ)*ABZN
567 VF=Z(2,KZ)*ABZN
568 WP=Z(3,KZ)*ABZN
569 WRITE(6,218) K, UP, VP, WP, X(1,K), X(2,K), X(3,K)
570 IF(.NOT.$PLOTS.OR..NOT.$MODAL.EC.0) GC TO 447
571 YL(K)=UP
572 YV(K)=VF
573 YFIS(K)=X(1,K)
574 YFIT(K)=X(2,K)
575 YFI(K)=X(3,K)
576 CCNTINUE
577 IF($FLCITS.AND.$MODAL.AND.((ICCHK1.GT.0).OR.(ICCHK2.GT.0)))
578 1 CALL PLOT2(1)
579 1 CCNTINUE
580 C*****
581 1C1 FCRMAT(1, 'THE LOAD STEP NUMBER IS ', I2, '
582 2 FCRMAT(2, 'THE SOLUTION CONVERGED IN ', I2, '
583 3 FCRMAT(3, 'ITERATIONS', '///')
584 116 1C FCRMAT(4, 'THE SUMMED FORCES, MOMENTS, DISPLACEMENTS ANS
585 117 1C FCRMAT(5, FOLLOW FOR THETA =', E15.6//') N S N THETA N STHETA

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SAT117120

31



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CCCMCN /BL3/ PR(99),PX(99),PT(99)
CCCMCN /BL4/ ZF1M(4,4,99),ZF2M(4,4,99),
1 ZF3M(4,4,99),ZF4M(4,4,99)
CCCMCN /BL5/ TT(99),MT(99),DT(99),DMT(99)
CCCMCN /BL6/ SQE,CSE,ALOAD
CCCMCN /BL7/ DI,SI
CCCMCN /BL8/ R(500),GAM(500),OMT(500)
CCCMCN /BL9/ FFS(4,99),ELIS(4),CEES(4,99)
CCCMCN /BL14/ LAM2,LSD18,LSDIN
CCCMCN /BL15/ NU,UI(99),VI(99),W1(99),V2(99),U2(99),W2(99),U3(99),
1 V3(99),W3(99)
CCCMCN /BL16/ VPS
CCCMCN /BL18/ ELI(4),ELL(4)
CCCMCN /BL27/ BXT3(99),BXT3(99),BE3(99)
CCCMCN /BL28/ EXX3(99),ETI3(99),ETI3(99),EX2(99),ETI3(99)
CCCMCN /BL29/ BXT1(99),BXT1(99),BXT1(99),EX2(99),BT2(99),
1 BXT2(99),BE2(99)
CCCMCN /BL30/ EXX1(99),ETI1(99),ETI1(99),EX1(99),ETI1(99),EXX2(99),
1 ETI2(99),ETI2(99),EX2(99),ETI2(99)
CCCMCN /BL31/ DELESQ,EXTI(99)
CCCMCN /BL100/ TEEEC,$DYNMC
CCCMCN /BL101/ DELSD
CCCMCN /BL102/ DELDAD
CCCMCN /BL103/ MASS(500)
1 DIMENSION ELLS(4),FLS(4),ZI(4),IPIVOT(4),INDEX(4,2)
2,CL2(4,4),CL1(4,4),ZDD(4)
1,CL2(4,4),CL1(4,4),ZDD(4)
C*****ECLIVALENCE*****
CC 201 I=1,4
CC 201 M=1,MNMAX
AJ=1+(M-1)*KMAX2
TZMAX(I,M)=ABS(Z(I,MJ))
CC 201 K=2,KMAX2
K=K+(M-1)*KMAX2
AZTST=ABS(Z(I,KM))
IF(AZTST.GT.TZMAX(I,M)) TZMAX(I,M)=AZTST
CCCONTINUE
2C1
IF(ITRMX.EQ.1) GC TC 66
DC 1 M=1,MNMAXO
I=1+(KMAX+2)*(M-1)
LI(M)=Z(1,I)
VI(M)=Z(2,I)
W1(M)=Z(3,I)
W2(M)=Z(1,I)
W2(M)=Z(2,I)
SAT17610
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SAT17660
SAT17670
SAT17690
SAT17700
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SAT17720
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 SAT118560

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1  W2(M)=Z(3,I1) GC TO 100
   IF(IBCINL.LT.0) GC TO 100
   CALL PHIBET(1,Z,IS,JS,ID,JD,PHIXE,PHITB)
   CC 2 P=1,MNMAX
   BT1(M)=BX3(M)
   BT11(M)=BT3(M)
   BX11(M)=BX3(M)
   BE1(M)=BE3(M)
   CALL TEAETA(1,Z,IS,JS,ID,JD)
   CC 3 M=1,MNMAX
   EXX1(M)=EXX3(M)
   ET11(M)=ETX3(M)
   EX11(M)=ETX3(M)
   EX1(M)=EX3(M)
   ET1(M)=ET3(M)
   CALL PHIBET(2,Z,IS,JS,ID,JD,PHIXE,PHITB)
   CC 4 P=1,MNMAX
   BX2(M)=BX3(M)
   ET2(M)=BT3(M)
   BE2(M)=BE3(M)
   CALL TEAETA(2,Z,IS,JS,ID,JD)
   CC 5 P=1,MNMAX
   EXX2(M)=EXX3(M)
   ETX2(M)=ETX3(M)
   EX2(M)=EX3(M)
   ET2(M)=ET3(M)
   CALL PHIBET(3,Z,IS,JS,ID,JD,PHIXB,PHITB)
   CCNT INUE
   IF(IBCINL.LT.0) GC TO 20
   CALL BDB(1,B1,DB,D,CD)
   GAM1=GAM(1)
   CALL TLCCAD(1,Z)
   CC 8 P=1,MNMAX
   IF(ITRMAX.EQ.1) GO TO 67
   FFS(1,M)=-TT(M)*ALCAD+OSE*(BX1(M)+BE1(M)+NU*(BT1(M)+BE1(M))*B1
   FFS(2,M)=OSE*(B1 *BT1(M)+EX1(M)+ET1(M))
   FFS(3,M)=LAM2*GAM1*DI*MT(M)*ALOAD-(EXX1(M)+ETX1(M))*SOE
   GO TO 8
   FFS(1,M)=-TT(M)*ALCAD
   FFS(2,M)=0.
   FFS(3,M)=LAM2*GAM1*DI*MT(M)*ALOAD
   FFS(4,M)=0.
   CC 9 I=1,4
  
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5      ELLS(I)=ALOAD*ELL(I)
20     CALL FORCE(1,P,X,DEE,DST,Z,ZO,Z2,Z3)
      CC 10 K=3,KLL
      KF=K+1
      IF(I,TRMAX.EQ.1) GO TO 1C
      CALL UPDATE
      CALL PHIBET(KP,Z,IS,JS,ID,JD,PHIXE,PHITB)
      CALL TEAETA(KP,Z,IS,JS,ID,JD)
      CALL FCRCE(K,P,X,DEE,DST,Z,ZO,Z2,Z3)
1C     IF(I,TRMAX.NE.1) CALL UPDATE
      IF(I,RCFNL.LT.0) GO TO 120
      IF(I,TRMAX.EQ.1) GO TO 11
      CALL PHIBET(KMAX,Z,IS,JS,ID,JD,PHIXB,PHITB)
      CALL TEAETA(KMAX,Z,IS,JS,ID,JD)
11     CALL FCRCE(KL,P,X,DEE,DST,Z,ZO,Z2,Z3)
      CC 12 I=1,4
      ELLS(I)=ALOAD*ELL(I)
      CALL BCB(KMAX,BL,DB,D,DD)
      GAML=GAM(KMAX)
      FLS(4)=C
      CALL TLCD(KMAX,Z)
      CC 14 M=1,MNMAX
      IF(M.GT.1) ELLS(I)=0.0
      IF(I,TRMAX.EQ.1) GO TO 68
      FLS(1)=-TT(M)*ALCD+OSE*(BX3(M)+BE3(M)+NU*(ET3(M)+BE3(M))*BL
      FLS(2)=OSE*(BL*DI*BT(M)*ALOAD-(EXX3(M)+ETX3(M))*SOE
      FLS(3)=LAM2*GAML*DI*MT(M)*ALOAD
      GO TO 65
      FLS(1)=-TT(M)*ALOAD
      FLS(2)=C
      FLS(3)=LAM2*GAML*DI*MT(M)*ALOAD
      CC 15 INUE
      IK=KL+KMAX*(M-1)
      IJ=KMAX*M
      L=N*KMAX2
      DC 14 I=1,4
      SUMZ=0.
      CC 15 J=1,4
      C*****
      C THE FOLLOWING CARD CAUSES BOUNDARY CONS TO EXIST FOR MODE 'O', ONLY
      C*****
      IF (M.NE.1) ELLS(J)=0
      IF SUMZ=SUMZ+ZF1M(I,J,M)*ELLS(J)+ZF2M(I,J,M)*X(J,IJ)+ZF3M(I,J,M)*
      15 IX(J,IK)+ZF4M(I,J,M)*FLS(J)
      14 Z(I,L)=SUMZ
      LS=I

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 SAT19040

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15C      CC 16 M=1, MNMAX
          CC 16 L=LS, KMAX
          K=KMAX2-L
          KFX=K-1
          KZ=K+1
          IJ=KFX+(H-1)*KMAX
          JM=KZ+(M-1)*KMAX2
          KK=JK-1
          CC 17 I=1,4
          SUMZ=0.
18      CC 18 J=1,4
          SUMZ=SUMZ-P(I,J,IJ)*Z(J,JK)
          ASUMZ=SUMZ+X(I,IJ)
          ASUMZ=ABS(SUMZ)
          IF(ASUMZ.GT.1.E+15) ITR=ITRMAX
          IF(NCCNV.NE.1.OR. ASUMZ.LT. 1.E-05) GC TC 17
          DELZ=ABS(Z(I,JK))-SUMZ
          ZTEST=EFS*IZMAX(I,M)
          IF(DEEZ.GT.ZTEST) NCONV=0
          Z(I,KK)=SUMZ
17      CC CONTINUE
16      IF(IBCINL.LT.0) GO TO 30
          CC 25 M=1, MNMAX
          CALL EFG(I,M,ZO,Z2,Z3)
          CALL ABC
          IJ=2+(M-1)*KMAX2
          I=IJ+1
          I2=IJ-1
          CC 21 I=1,4
          SUMZ=0.
          CC 22 J=1,4
          SUMZ=SUMZ-A(I,J)*Z(J,IJ)-BEE(I,J)*Z(J,IJ)
          ZT(I)=SUMZ+GEES(I,M)
          CC 21 CALL MATINV(C,4,ZI,I, DETERM, IPIVOT, INDEX,4, ISCALE)
          CC 23 I=1,4
          Z(I,IJ2)=ZT(I)
          CC CONTINUE
          RETURN
100      CALL INLPOL (Z,PHIXB,PHITB)
          CC 101 M=1, MNMAX
          U1(M)=U2(M)
          V1(M)=V2(M)
          W1(M)=W2(M)
          I=3+KMAX2*(M-1)
          U2(M)=Z(1,IJ)
          V2(M)=Z(2,IJ)
          W2(M)=Z(3,IJ)
          CC 102
          GC TC IC2

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SAT19510
SAT19520

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120 IF (ITRMAX.NE.1) CALL FALPOL (Z,PTIXB,PHITB)
    CALL FCRCE(KL,P,X,DEE,DST,Z,ZC,Z2,Z3)
    IF (M2.EC.0) GO TO 122
    L=KL+(M2-1)*KMAX
    L1=KMAX1+(M2-1)*KMAX2
    CC 130 I=1,4
    SUM=0.
    CC 131 J=1,4
    SUM=SUM+CLC(I,J)*X(J,L)
    ASUMZ=ABS(SUM)
    IF (NCONV.NE.1 .OR. ASUMZ.LT.1.E-05) GO TC 130
    DELZ=ABS(Z(I,L1)-SUM)
    ZTEST=EPS*IZMAX(I,M2)
    IF (DELZ.GT.ZTEST) NCONV=0
    Z(I,L1)=SUM
    IF (M1.EC.0) GO TO 123
    L=KL+(M1-1)*KMAX
    L1=KMAX1+(M1-1)*KMAX2
    CC 132 I=1,4
    SUM=0.
    CC 133 J=1,4
    SUM=SUM+CLC(I,J)*X(J,L)
    ASUMZ=ABS(SUM)
    IF (NCONV.NE.1 .OR. ASUMZ .LT. 1.E-05) GO TC 132
    DELZ=ABS(Z(I,L1)-SUM)
    ZTEST=EPS*IZMAX(I,M1)
    IF (DELZ.GT.ZTEST) NCONV=0
    Z(I,L1)=SUM
    IF (M0.EC.0) GO TO 124
    L=KL+(M0-1)*KMAX
    L1=KMAX1+(M0-1)*KMAX2
    CC 134 I=1,4
    SUM=0.
    CC 135 J=1,4
    SUM=SUM+CLC(I,J)*X(J,L)
    ASUMZ=ABS(SUM)
    IF (NCONV.NE.1 .OR. ASUMZ.LT.1.E-06) GO TC 134
    DELZ=ABS(Z(I,L1)-SUM)
    ZTEST=EPS*IZMAX(I,M0)
    IF (DELZ.GT.ZTEST) NCONV=0
    Z(I,L1)=SUM
    L1=2
    CC 136 TO 150
    ENCL
    SLROUTINE PLOT2(NTH)
    *****
    C ***** THIS SUBROUTINE CALLS PLOTTING ROUTINES FOR APPROPRIATE (USER *****
    C ***** SATI20000

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SATI19990
SATI20000

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      9      WRITE (6,1006) TH(NTH)
      IF (IMSTH.EQ.0) GO TO 1211
      WRITE (6,1000)
      IF (IMSTH.GT.0) CALL PLOTIT (XSTATN,YMSTH,KMAX,0)
      IF (IMSTH.LT.0) CALL PLOTIT (XSTATN,YMSTH,NGKMAX,0)
      1211  IF (IU.EQ.0) GO TO 10
      WRITE (6,1007) TH(NTH)
      IF (IU.EQ.0) GO TO 10
      WRITE (6,1000)
      IF (IU.GT.0) CALL PLOTIT (XSTATN,YU,KMAX,0)
      IF (IU.LT.0) CALL PLOTIT (XSTATN,YU,NGKMAX,C)
      10      WRITE (6,1010) TF(NTH)
      IF (IV.EQ.0) GO TO 11
      IF (IV.EQ.C) GO TO 11
      10      WRITE (6,1000)
      IF (IV.GT.0) CALL PLOTIT (XSTATN,YV,KMAX,C)
      IF (IV.LT.0) CALL PLOTIT (XSTATN,YV,NGKMAX,C)
      11      WRITE (6,1009) TH(NTH)
      IF (IW.EQ.0) GO TO 12
      IF (IW.EQ.0) GO TO 12
      11      WRITE (6,1000)
      IF (IW.GT.0) CALL PLOTIT (XSTATN,YW,KMAX,0)
      IF (IW.LT.0) CALL PLOTIT (XSTATN,YW,NGKMAX,0)
      12      WRITE (6,1008) TF(NTH)
      IF (IPHIS.EQ.0) GO TO 13
      IF (IPHIS.EQ.0) GO TO 13
      12      WRITE (6,1000)
      IF (IPHIS.GT.0) CALL PLOTIT (XSTATN,YPHIS,KMAX,0)
      IF (IPHIS.LT.0) CALL PLOTIT (XSTATN,YPHIS,NGKMAX,0)
      13      WRITE (6,1011) TH(NTH)
      IF (IPHI.EQ.0) GO TO 14
      IF (IPHI.EQ.0) GO TO 14
      13      WRITE (6,1000)
      IF (IPHI.GT.0) CALL PLOTIT (XSTATN,YPHI,KMAX,0)
      IF (IPHI.LT.0) CALL PLOTIT (XSTATN,YPHI,NGKMAX,0)
      14      WRITE (6,1012) TH(NTH)
      IF (IPHI.EQ.0) GO TO 21
      IF (IPHI.EQ.0) GO TO 21
      14      WRITE (6,1000)
      IF (IPHI.GT.0) CALL PLOTIT (XSTATN,YPHI,KMAX,0)
      IF (IPHI.LT.0) CALL PLOTIT (XSTATN,YPHI,NGKMAX,0)
      21      WRITE (6,1013) TH(NTH)
      RETURN
      121  IF (INS.EQ.0) GO TO 15
      IF (INS.EQ.0) GO TO 15
      121  WRITE (6,1000)
      IF (INS.GT.0) CALL PLOTIT (XSTATN,YNS,KMAX,C)
      IF (INS.LT.0) CALL PLOTIT (XSTATN,YNS,NGKMAX,0)
      15      WRITE (6,2001)
      IF (INTF.EQ.0) GO TO 16
      IF (INTF.EQ.0) GO TO 16
      15      WRITE (6,1000)
      IF (INTF.GT.0) CALL PLOTIT (XSTATN,YNTH,KMAX,0)
      IF (INTF.LT.0) CALL PLOTIT (XSTATN,YNTH,NGKMAX,0)
      16      WRITE (6,2002)
      IF (INSTH.EQ.0) GO TO 17
      IF (INSTH.EQ.0) GO TO 17

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17 WRITE (6,1000) CALL PLCTIT (XSTAIN,YNSTH,KMAX,0)
   IF (INSTH.GT.0) CALL PLCTIT (XSTAIN,YNSTH,NGKMAX,0)
   WRITE (6,2003) GO TO 18
   IF (ICS.EQ.0) GO TO 18
   WRITE (6,1000)
   IF (IQS.GT.0) CALL PLCTIT (XSTAIN,YQS,KMAX,C)
   IF (IQS.LT.0) CALL PLCTIT (XSTAIN,YQS,NGKMAX,C)
18 WRITE (6,2004) GO TO 19
   IF (IMS.EQ.0) GO TO 19
   WRITE (6,1000)
   IF (IMS.GT.0) CALL FLOIT (XSTAIN,YMS,KMAX,C)
   IF (IMS.LT.0) CALL FLOIT (XSTAIN,YMS,NGKMAX,C)
19 IF (IMTH.EQ.0) GO TO 22
   WRITE (6,2005)
   IF (IMTH.GT.0) CALL FLOIT (XSTAIN,YMTH,KMAX,C)
   IF (IMTH.LT.0) CALL FLOIT (XSTAIN,YMTH,NGKMAX,C)
22 WRITE (6,2006) GO TO 231
   IF (IMSTH.EQ.0) GO TO 231
   WRITE (6,1000)
   IF (IMSTH.GT.0) CALL PLCTIT (XSTAIN,YMSTH,KMAX,0)
   IF (IMSTH.LT.0) CALL PLCTIT (XSTAIN,YMSTH,NGKMAX,0)
231 IF (IU.EQ.0) GO TO 23
   WRITE (6,2007)
   IF (IU.GT.0) CALL PLCTIT (XSTAIN,YU,KMAX,C)
   IF (IU.LT.0) CALL PLCTIT (XSTAIN,YU,NGKMAX,C)
23 IF (IV.EQ.0) GO TO 24
   WRITE (6,1000)
   IF (IV.GT.0) CALL PLCTIT (XSTAIN,YV,KMAX,C)
   IF (IV.LT.0) CALL PLCTIT (XSTAIN,YV,NGKMAX,C)
24 IF (IW.EQ.0) GO TO 25
   WRITE (6,2009)
   IF (IW.GT.0) CALL PLCTIT (XSTAIN,YW,KMAX,C)
   IF (IW.LT.0) CALL PLCTIT (XSTAIN,YW,NGKMAX,C)
25 IF (IPHS.EQ.0) GO TO 26
   WRITE (6,1000)
   IF (IPHS.GT.0) CALL PLCTIT (XSTAIN,YPHIS,KMAX,0)
   IF (IPHS.LT.0) CALL PLCTIT (XSTAIN,YPHIS,NGKMAX,0)
26 IF (IPHIT.EQ.0) GO TO 27
   WRITE (6,2011)
   IF (IPHIT.GT.0) CALL PLCTIT (XSTAIN,YPHIT,KMAX,0)
   IF (IPHIT.LT.0) CALL PLCTIT (XSTAIN,YPHIT,NGKMAX,0)

```

SAT2097C  
 SAT20980  
 SAT20990  
 SAT21000  
 SAT21010  
 SAT21020  
 SAT21030  
 SAT21040  
 SAT21050  
 SAT21060  
 SAT21070  
 SAT21080  
 SAT21090  
 SAT21100  
 SAT21110  
 SAT21120  
 SAT21130  
 SAT21140  
 SAT21150  
 SAT21160  
 SAT21170  
 SAT21180  
 SAT21190  
 SAT21200  
 SAT21210  
 SAT21220  
 SAT21230  
 SAT21240  
 SAT21250  
 SAT21260  
 SAT21270  
 SAT21280  
 SAT21290  
 SAT21300  
 SAT21310  
 SAT21320  
 SAT21330  
 SAT21340  
 SAT21350  
 SAT21360  
 SAT21370  
 SAT21380  
 SAT21390  
 SAT21400  
 SAT21410  
 SAT21420  
 SAT21430  
 SAT21440



```

27 WRITE (6,2C12) GO TO 28
   IF (IPHI.EQ.0)
   WRITE (6,1000)
   IF (IPHI.GT.0) CALL PLCTIT (XSTATN,YPHI ,KMAX,0)
   IF (IPHI.LT.0) CALL PLOTIT (XSTATN,YPHI ,NCKMAX,0)
   RETURN
28 *****
1000 FCRMAT (1,1) T10,"S"-MEMBRANE FCRC VS STATN, MERIDIAN AT THETA =
1001 FCRMAT (1,0,"RADIANS")
1002 FCRMAT (1,0,"RADIANS")
1003 FCRMAT (1,0,"RADIANS")
1004 FCRMAT (1,0,"RADIANS")
1005 FCRMAT (1,0,"RADIANS")
1006 FCRMAT (1,0,"RADIANS")
1007 FCRMAT (1,0,"RADIANS")
1008 FCRMAT (1,0,"RADIANS")
1009 FCRMAT (1,0,"RADIANS")
1010 FCRMAT (1,0,"RADIANS")
1011 FCRMAT (1,0,"RADIANS")
1012 FCRMAT (1,0,"RADIANS")
1013 FCRMAT (1,0,"RADIANS")
2001 FCRMAT (1,0,"RADIANS")
2002 FCRMAT (1,0,"RADIANS")
2003 FCRMAT (1,0,"RADIANS")
2004 FCRMAT (1,0,"RADIANS")
2005 FCRMAT (1,0,"RADIANS")
2006 FCRMAT (1,0,"RADIANS")
2007 FCRMAT (1,0,"RADIANS")
2008 FCRMAT (1,0,"RADIANS")
2009 FCRMAT (1,0,"RADIANS")
2010 FCRMAT (1,0,"RADIANS")
2011 FCRMAT (1,0,"RADIANS")
2012 FCRMAT (1,0,"RADIANS")
2013 FCRMAT (1,0,"RADIANS")

```









AD-A035 911

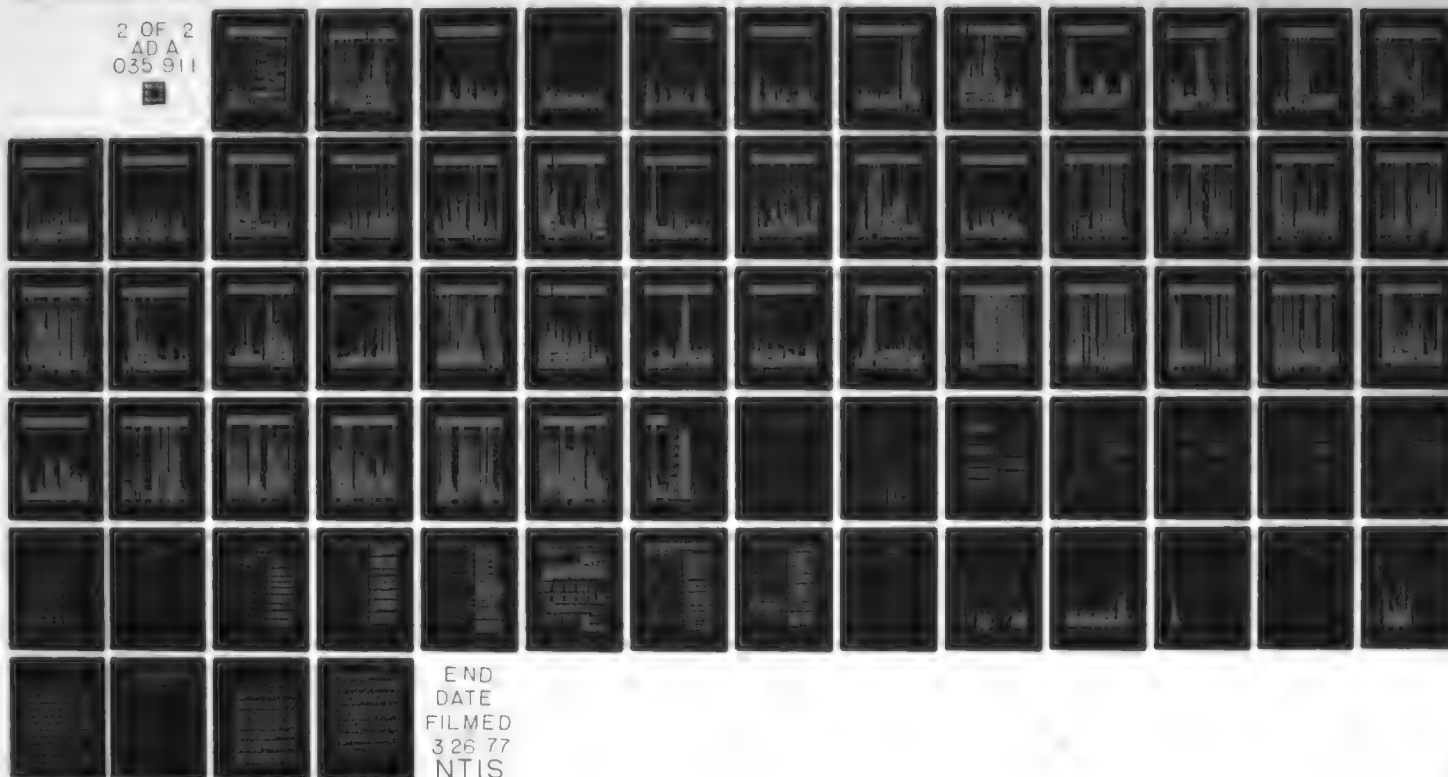
NAVAL POSTGRADUATE SCHOOL MONTEREY CALIF  
STATIC AND DYNAMIC BUCKLING OF SHALLOW SPHERICAL SHELLS SUBJECT--ETC(U)  
DEC 76 M D SHUTT

F/G 20/11

UNCLASSIFIED

NL

2 OF 2  
AD A  
035 911



```

20 FCRMAT ( , , , T11 , ,
X00 X X X OOX
000 )
21 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
22 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
23 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
24 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
25 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
26 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
27 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
28 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
29 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
30 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
31 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
32 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
33 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
34 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
35 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
36 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
37 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
38 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
39 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
40 FCRMAT ( , , , T11 , ,
X0C X X OOX
0000 )
RETURN
END
SUBROUTINE PMATRIX ( P,X,Z0,Z2,Z3,CSE,DST )
C*****
C***** THIS SUBROUTINE CALLS THE SUBROUTINES FJ(K,MN), EFG(K,MN), ABC,00001310
C*****

```



```

CCCCCCCCCCCCCCCC
AND PANDD(K,MN) TO SET UP THE P, P-BAR AND P-HAT MATRICES GIVEN
BY EQUATIONS (3C).
INTERNALLY, MATRICES DL, DG AND DF ARE SET UP FOR THE CALCULA-
TION OF X(I) GIVEN BY EQUATION (31A), WHERE
X(I) = OL*SMALL-L(I) + DG*SMALL-G(I) + DF*SMALL-F(I)
THE SPECIAL P MATRIX FOR A SHELL WITH AN INITIAL FCLE IS ALSO
COMPLETED HERE.
MATRICES ZF1M, ZF2M, ZF3M, ZF4M ARE SET UP FOR THE CALCULATION OF
Z(K+1) GIVEN BY EQUATION (31B), WHERE
Z(K+1)=ZF1M*SMALL-L(K) + ZF2M*X(K) + ZF3M*X(K-1) + ZF4M*SMALL-
IF THE SHELL HAS A FINAL POLE, THE MATRICES CLC, CL1, CL2 ARE
PREPARED FOR THE CALCULATION OF Z(K)
*****
REAL JAY
1 JIPENSICN P(4,4,1), DEE(4,4,1), DST(4,4,1), X(4,1), ZC(4,1),
1 Z2(4,1), Z3(4,1) MNMAX
1 CCMCN /BL1/ MNMAX
CCMCN /BL2/ N(95), MNINIT
CCMCN /BL3/ MO, M1, M2, M3
CCMCN /BL4/ KMAX, KL
CCMCN /BL5/ IBCINL, IBCFNL
CCMCN /BL1/ A(4,4), BEE(4,4,99), ZF2M(4,4,99),
CCMCN /BL4/ ZF1M(4,4,99), ZF4M(4,4,99),
1 CCMCN /BL13/ OMEGL(4,4), CAPL1(4,4), OMEGL(4,4), CAPLL(4,4),
1 CCMCN /BL23/ JAY(4,4), F(4,4)
CCMCN /BL24/ DL(4,4,99), DG(4,4,99), DF(4,4,99)
CCMCN /BL25/ E(4,4), PBT(4,4), G(4,4)
1 JIPENSICN PATA(4,4,4), ZF2(4,4,4), ZFPG(4,4), ZFP2(4,4), PIR(4,
14), CGG(4,4), ZF1(4,4), ZF2(4,4), CL1(4,4), CL2(4,4), G1(4,
214), INCEX(4,2), CLO(1), ZF1M(1), PBT(1), ZF2M(1), (CL2(1), ZF3M(1)),
ECLIVALENCE(CLO(1), ZF1(1), ZF2(1), PIR(1))
1 (ZFPO(1), PATA(1), ZF1(1), ZF2(1))
2 (ZF1(1), DLL(1), ZF2(1))
*****
IF (IBCINL-LT-0) GO TO 10
CC 1 PA=MNINIT, MNMAX
CC 1 FJ(1, MN)
CALL EFC(1, MN, ZO, Z2, Z3)
CALL ABC
CALL MATINV(C,4,G1,0, DETERM, IPIVGT, INDEX,4, ISCALE)
CC 3 J=1,4
CC 3 J=1,4
*****
00001600
00001610
00001620
00001640
00001650
00001660
00001670
00001680
00001690
0001700
00001710
00001720
00001730
00001740
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00001770
00001780
00001790

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```

TTC=0.
CC SC6 L=1,4
TTF=TP+CL0(I,I,L)*C(L,JJ)
TTC=TTQ+CL0(I,I,L)*BEE(L,JJ)
CL1(I,I,JJ)=DL(I,I,JJ,MN)-TTP
CL2(I,I,JJ)=DG(I,I,JJ,MN)-TTP
CALL MATINV(CLI,4,GI,0,DETERM, IPIVOT, INDEX,4, ISCALE)
CC SC7 I=1,4
CC SC7 JJ=1,4
TTP=0.
TTC=0.
CC SC8 L=1,4
TTF=TP+CL1(I,I,L)*CL0(L,JJ)
TTC=TTQ+CL1(I,I,L)*CL2(L,JJ)
CL(I,I,JJ,MN)=-TTP
P(I,I,JJ,IJ)=TTQ
MN=MNNU
CC SC9 CCNIT=KMAX
IF(IBCFL.LT.0) KLAST=KL
CC 23 K=2, KLAST
CC 23 MN=MNINIT, MNMAX
CALL EFC(K,MN,Z0,Z2,Z3)
CALL ABC
CALL FAN DD(K,MN,P,CEE,DST,X)
IF(IBCFL.LT.0) GC TO 30
CC 40 MN=MNINIT, MNMAX
IKL=MN*KMAX-1
CALL FJ(KMAX,MN)
CC 41 I=1,4
CC 41 J=1,4
SUMC=0.
SUMF=0.
SUMJ=0.
L=1,4
SUMC=SUMC+P(I,I,IKL)*F(L,J,JKL)
SUMF=SUMF+SUMJ+GMEGL(I,L)*JAY(L,J)
PATA(I,J)=SUMC
PETA(I,J)=UNIT(I,J)-SUMF
PETA(I,J)=SUMJ+CAPLL(I,J)
CC 43 I=1,4
CC 43 J=1,4
SUMCP=0.
SUMJP=0.
SUMCM=0.

```

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00002430
00002440
00002440
00002450
00002460
00002470
00002480
00002490
00002500
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00002560
00002570
00002580
00002590
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00002670
00002680
00002690
00002700
00002710
00002720

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0000273C  
00002740  
00002750  
00002760  
00002770  
00002780  
00002790  
00002800  
00002810  
00002820  
00002830  
00002840  
00002850  
00002860  
00002870  
00002880  
00002890  
00002900  
00002910  
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00002960  
00002970  
00002980  
00002990  
00003000  
00003010  
00003020  
00003030  
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00003060  
00003070  
00003080  
00003090  
00003100  
00003110  
00003120  
00003130  
00003140  
00003150  
00003160  
00003170  
00003180  
00003190  
00003200

```

44 44 L=1,4
SUMOP=SUMOP+PATA(I,L)*PBTA(L,J)
SUMJP=SUMJP+PATA(I,L)*P(L,J,JKL)
SUMCM=SUMCM-PATA(I,L)*P(L,J,IKL)
43 ZF1(I,J)=SUMOP-SUMJP
ZF2(I,J)=SUMCM-PJTA(I,J)
CALL MATINV(ZF1,4,ZF2,4,DETERM,IFIVOT,INDEX,4,ISCALE)
44 45 I=1,4
45 45 J=1,4
ZF3=0.
ZF4=0.
46 46 L=1,4
ZF3=SZF3+ZF1(I,L)*PATA(L,J)
ZF4=SZF4-ZF1(I,L)*CMEGL(L,J)
45 ZF3M(I,J,MN)=SZF3
45 ZF4M(I,J,MN)=SZF4
45 ZF1M(I,J,MN)=ZF1(I,J)
45 ZF2M(I,J,MN)=ZF2(I,J)
45 45 CCNTINUE
45 45 RETURN
45 45 MN=MNINIT,MNMAX
45 45 IKL=MN*MKMAX-1
45 45 NN=N(MN)
45 45 NN=IABS(N(MN))
45 45 IF(NN.GT.3) GO TO 31
45 45 IF(NN.GT.2) GO TO 300
45 45 IF(NN.GT.1) GO TO 33
45 45 IF(NN.GT.0) GC TO 34
45 45 NC=MN
45 45 J=1,4
45 45 I=1,4
45 45 J=0.
45 45 CLC(I,J)=0.
45 45 ZFPC(I,J)=1.
45 45 ZFFC(1,2)=1.
45 45 ZFFC(3,1)=P(3,1,IKL)
45 45 ZFFC(3,2)=P(3,2,IKL)+1.
45 45 ZFFC(3,3)=P(3,3,IKL)
45 45 ZFFC(3,4)=P(3,4,IKL)
45 45 ZFFC(4,1)=P(4,1,IKL)
45 45 ZFFC(4,2)=P(4,2,IKL)
45 45 ZFFC(4,3)=P(4,3,IKL)
45 45 ZFFC(4,4)=P(4,4,IKL)+1.
45 45 CLC(3,3)=1.
45 45 CLC(4,4)=1.
45 45 CALL MATINV(ZFPO,4,CLO,4,DETERM,IFIVOT,INDEX,4,ISCALE)
45 45 GC TO 31
45 45 NC=MN
3CC 3CC

```



```

CCMCMCN /BL5/ IBCINL, IBCFNL
CCMCMCN /BL8/ LSTEP, ITR
CCMCMCN /BL12/ KMAX1, KMAX2, NCONV
CCMCMCN /BL13/ ITRMAX, LSMAX
CCMCMCN /BL3/ PR(99), PX(99), PT(99)
CCMCMCN /BL4/ ZF1M(4,4,99), ZF2M(4,4,99),
1 ZF3M(4,4,99), ZF4M(4,4,99)
CCMCMCN /BL5/ ZT(99), MI(99), DT(99), DMT(99)
CCMCMCN /BL6/ SOE, QSE, ALOAD
CCMCMCN /BL7/ DI, S1
CCMCMCN /BL8/ R(500), GAM(500), QMT(500)
CCMCMCN /BL9/ RFS(4,99), ELIS(4), GEES(4,99)
CCMCMCN /BL11/ OMXI(500), PHEE, TO, T2
CCMCMCN /BL12/ TDLI, TDEL
CCMCMCN /BL14/ LAM2, LSD18, LSDIN
CCMCMCN /BL15/ NU, UI(99), V1(99), W1(99), V2(99), U2(99), W2(99), U3(99),
1 V3(99), W3(99)
CCMCMCN /BL17/ DEL
CCMCMCN /BL24/ DL(4,4,99), DG(4,4,99), DF(4,4,99)
CCMCMCN /BL27/ BX3(99), BT3(99), BXT3(99), BE3(99)
CCMCMCN /BL28/ EXX3(99), ET13(99), ETX3(99), EX2(99), ET2(99),
CCMCMCN /BL29/ BX1(99), BT1(99), BXT1(99), BE1(99), BX2(99), B12(99),
1 BXT2(99), BE2(99)
CCMCMCN /BL30/ EXX1(99), ET11(99), ETX1(99), EX1(99), ET1(99), EXX2(99),
1 ET2(99), ETX2(99), EX12(99), EX2(99), ET2(99)
CCMCMCN /BL31/ DELSC, EX11(99)
CCMCMCN /BL100/ TEEC, $DYNMC
CCMCMCN /BL101/ DELSD
CCMCMCN /BL102/ DELQAD
CCMCMCN /BL103/ MASS(500)
CCMCMCN /BL104/ GEE(4)
DIMENSION GEE(4)
C*****FCIFF(A,B,C)=(-1.5*A+2.*B-.5*C)/DEL
RS=R(K)
RF=1./RS
GA=GAM(K)
GX=CMT(K)
CT=CMT(K)
L12=DI*LAM2
CALL PLCAD(K,BS,DBS,D,DD)
CALL TLCCAD(K,Z)
MASS=MASS(K)
LC 4 F=1,MMAX
I2=K+1+(M-1)*KMAX
IK=K+(M-1)*KMAX
EN=N(N)
00003690
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00003990
00004000
00004010
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00004120
00004130
00004140
00004150

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000004620  
000004630

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C**      CXX=-FCLIFF(EXX2T,EXX2(M),EXX1(M))
C**      CDET=-FCDIFF(ETX2T,ETX2(M),ETX1(M))
C**      CC TO 7
C**      CBX=TDLI*(BX3(M)-BX1(M))
C**      CBEL=TDCLI*(BT3(M)-BT1(M))
C**      CBET=TDCLI*(BE3(M)-BE1(M))
C**      CBXT=TDCLI*(BXT3(M)-BXT1(M))
C**      CCEX=TDCLI*(ET3(M)-ET1(M))
C**      CEEX=TDCLI*(EX3(M)-EX1(M))
C**      CEEXX=TDCLI*(EXX3(M)-EXX1(M))
C**      CBXT2T=BX2(M)
C**      BEXT2T=BT2(M)
C**      BEXT2T=BE2(M)
C**      EEXT2T=ET2(M)
C**      EXXT2T=EX2(M)
C**      ET2T=ET2(M)
C**      GEE(1)=GEE(1)+ENR*DI#BS*(BS*(CBX+CBE+GA*D1*(BX2T-ET2T)+NU*(CBT+CBE)
C**              +ENR*DI#BS*(BXT2T+ETX2T)+NU*(BT2T+BE2T))-2.*CX*
C**              (EXX2T+ETX2T)-ENR*(EX2T+ET2T))*TDEL
C**      GEE(2)=GEE(2)+OSE*(BS*(ENR*(BT2T+BE2T)+NU*(BXT2T+BE2T))-D1*
C**              (CBX+D2.*GA*BXT2T))-D1*DBS*BXT2T+2.*CT*(ETT2T+EXT2T)
C**              -(DEX+DET))*TDEL
C**      GEE(3)=GEE(3)+OSE*(BS*(OX+NU*GT)*(BX2T+BE2T)+(OT+NU*QX)*
C**              (BT2T+BE2T))+2.*(GA*(EXX2T+ETX2T)+CEXX+DET*ENR*
C**              (EXT2T+ETT2T))*TDEL
C**      IF(K.GT.1) GO TO 10
C**      IF(M.GT.1) ELIS(1)=0.0
C**      CCES(I,M)=GEE(I)
C**      SUMX=0.
C**      CC 21 J=1,4
C**      FLOWING CARD CAUSES A SPECIFIED BCUNDARY CCNDITION VALUE TC
C**      EXISTS ONLY FOR MCDE'0.
C**      IF (M.NE.1) ELIS(J)=0.
C**      SUMX=SUMX+GL(I,J,M)*ELIS(J)+DG(I,J,M)*GEE(J)+DF(I,J,M)*FFS(J,M)
C**      21 X(I,IK)=SUMX
C**      22 X(I,IG)=4
C**      IN FCRCNE
C**      IC IF(K.NE.2.OR.(K.EQ.2.ANC.IBCINL.GE.O)) GC TC 501
C**      SUMX=0.

```





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00005690
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00005980
00005990

RETURN
END
SUBROUTINE MATINV(A,N,B,M,DETERM,IPIVOT,INDEX,NMAX,ISCALE)
*****
THIS SUBROUTINE SOLVES THE MATRIX EQUATION AX=B, WHERE A IS
A SQUARE COEFFICIENT MATRIX AND B IS A MATRIX OF CONSTANT VEC-
TORS.
A(INVERSE) IS ALSO OBTAINED AND THE DETERMINANT OF A IS AVAIL-
ABLE.
THE FOLLOWING MUST BE DIMENSIONED IN THE CALLING PROGRAM:
IPIVOT(N MAX), INDEX(N MAX,2), A(N MAX,N MAX), B(N MAX,N MAX)
WHERE:
A = NAME OF 2-DIMENSIONAL ARRAY TO BE INVERTED
N = ORDER OF A - 1<=N<=NMAX
B = NAME OF 2-DIMENSIONAL ARRAY TO BE MULTIPLIED
BY A(INVERSE)
M = NUMBER OF COLUMN VECTORS IN B
NOTE: M = 0 SIGNALS INVERSION ONLY
IPIVOT = TEMPORARY STORAGE BLOCK
INDEX = TEMPORARY STORAGE BLOCK
NMAX = MAXIMUM ORDER OF A (AS DIMENSIONED IN THE
CALLING PROGRAM)
DETERM= VALUE OF DETERMINANT AS GIVEN BELOW
ISCALE = USED IN FORMULA BELOW
DETERMINANT(A) = (IC*18)**ISCALE*(DETERM)
A(INVERSE) IS STORED IN A
A(INVERSE)*B IS STORED IN B
*****
DIMENSION IPIVOT(N),A(NMAX,N),B(NMAX,M),INDEX(NMAX,2)
EQUIVALENCE(IPIVOT,IROW),JRCW), (ICOL,JCCOLUM), (AMAX,I,SKAP)
*****
INITIALIZATION
*****
ISCALE=C
R1=10.0**18
R2=1.0/R1
DETERM=1.0
DO 20 J=1,N
IF IPIVOT(J)=0
DO 550 I=1,N
*****
SEARCH FOR PIVOT ELEMENT
*****
AMAX=0.0
DO 105 J=1,N
DO 105 IF (IPIVOT(J)-1) 60, 105, 60

```

```

1000 CC 100 K=1,N
1001 IF (IPIVOT(K)-1) 80, 100, 740
1002 IF (ABS(AMAX)-ABS(A(J,K))) 85, 100, 100
1003 IF CM=J
1004 ICCLUM=K
1005 AMAX=A(J,K)
1006 CC CONTINUE
1007 CC CONTINUE
1008 IF IPIVOT(ICCLUM)=IPIVOT(ICOLUM)+1
1009
1010 INTERCHANGE ROWS TO PUT PIVOT ELEMENT ON DIAGONAL
1011
1012 IF (IROW-ICOLUM) 140, 260, 140
1013 LETERM=-DETERM
1014 CC 200 L=1,N
1015 SWAP=A(IROW,L)
1016 IF (IROW,L)=A(ICOLUM,L)
1017 A(ICOLUM,L)=SWAP
1018 IF (M) 260, 260, 210
1019 CC 250 L=1,M
1020 SWAP=B(IROW,L)
1021 IF (IROW,L)=B(ICOLUM,L)
1022 B(ICOLUM,L)=SWAP
1023 INDEX(I,1)=IROW
1024 INDEX(I,2)=ICOLUM
1025 PIVCT=A(ICCLUM,ICCLUM)
1026
1027 SCALE THE DETERMINANT
1028
1029 PIVCTI=PIVCT
1030 IF (ABS(DETERM)-R1) 1030, 1010, 1010
1031 CETERM=DETERM/R1
1032 ISCALE=ISCALE+1
1033 IF (ABS(DETERM)-R1) 1060, 1020, 1020
1034 CETERM=DETERM/R1
1035 ISCALE=ISCALE+1
1036 CC TO 1060
1037 IF (ABS(DETERM)-R2) 1040, 1040, 1060
1038 CETERM=DETERM*R1
1039 ISCALE=ISCALE-1
1040 IF (ABS(DETERM)-R2) 1050, 1050, 1060
1041 CETERM=DETERM*R1
1042 ISCALE=ISCALE-1
1043 IF (ABS(PIVCTI)-R1) 1090, 1070, 1070
1044 PIVCTI=PIVCTI/R1
1045 ISCALE=ISCALE+1
1046 IF (ABS(PIVCTI)-R1) 1320, 1080, 1080
1047 PIVCTI=PIVCTI/R1

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1050 ISCALE=ISCALE+1
1060 GC TO 320
1070 IF (ABS(PIVOTI)-R2) 200C, 2000, 320
1080 PIVCTI=PIVCTI+R1
1090 ISCALE=ISCALE-1
1100 IF (ABS(PIVCTI)-R2) 2010, 201C, 320
1110 PIVCTI=PIVCTI+R1
1120 ISCALE=ISCALE-1
1130 CETERN=ETERM*PIVOTI
1140
1150 DIVIDE PIVCT ROW BY PIVCT ELEMENT
1160
1170 A(ICOLU, ICCLUM)=1.0
1180 DC 350 L=1, N
1190 A(ICOLU, L)=A(ICOLU, L)/PIVOT
1200 IF (M) 380, 380, 360
1210 DC 370 L=1, M
1220 E(ICOLU, L)=B(ICOLU, L)/PIVCT
1230
1240 REDUCE NON-PIVOT ROWS
1250
1260 DC 550 L=1, N
1270 IF (L1-ICOLU) 400, 55C, 400
1280 T=A(L1, ICOLU)
1290 A(L1, ICCLUM)=0.0
1300 DC 450 L=1, N
1310 A(L1, L)=A(L1, L)-A(ICCLUM, L)*T
1320 IF (M) 500, 550, 460
1330 DC 500 L=1, M
1340 B(L1, L)=B(L1, L)-B(ICCLUM, L)*T
1350 CCNTINUE
1360
1370 INTERCHANGE COLUMNS
1380
1390 DC 710 I=1, N
1400 L=N+1-I
1410 IF (INDEX(L, 1)-INDEX(L, 2)) 630, 710, 630
1420 JFCW=INDEX(L, 1)
1430 JCCLUM=INDEX(L, 2)
1440 DC 705 K=1, N
1450 SWAP=A(K, JROW)
1460 A(K, JROW)=A(K, JCCLUM)
1470 JCCLUM=INDEX(L, 2)
1480 CCNTINUE
1490 RETURN
1500 ENCL
1510 SUBROUTINE INLPGL (Z, P-IXB, PHITB)

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C *****
C THIS SUBROUTINE COMPUTES THE NCN-LINEAR TERMS BETA-SUB S; AT AN
C -SLB THETA, -SUB S-THETA, ETA-SUB S-S AND -SUB THETA-S AT AN
C INITIAL POLE.
C *****
C DIMENSION Z(4,1), PHIXB(1), PHITB(1)
C COMMON /IBL1/ MNMAX
C COMMON /IBL3/ M0,M1,M2,M3
C COMMON /IBL12/ KMAX1,KMAX2,NCCNV
C COMMON /IBL13/ ITRMAX,LSMAX
C /IBLJ/ JUMP
C COMMON /BL5/ TT(55),EMT(99),DT(55),DMT(55)
C COMMON /BL6/ SOE,CSE,ALOAD
C COMMON /BL7/ DI,S1
C COMMON /BL11/ OMXI(200),PHEE,TO,T2
C COMMON /BL11A/ PHEEN,T2N
C COMMON /BL17/ DEL
C COMMON /BL29/ BXL(99),BT1(99),BX1(99),BX2(95),BT2(99),
C /BL30/ BXT2(99),BE2(99)
C /BL31/ EXXI(99),ET1(99),EX1(99),ET1(99),EXX2(99),
C /BL31/ ETI2(99),ETX2(99),ETI2(99),ETX2(99)
C /BL31/ DELSC,EXI1(99)
C *****
C CC1 MN=1,MNMAX
C BT1 (MN)=0.
C BXT1 (MN)=0.
C BEI (MN)=0.
C ETI1 (MN)=0.
C EXXI1 (MN)=0.
C IF (M1.EQ.0) RETURN
C I2=2+(M1-1)*KMAX2
C I3=I2+1
C I4=I3+1
C IF (JUMP.EQ.2) GO TO 1000
C PHEE=(1.5*Z(3,I2)-2.*Z(3,I3)+.5*Z(3,I4))/CEL+CMXI(1)*Z(1,I2)
C BET=5*PHEE**2
C IF (ITRMAX.EQ.1) BET=0.
C I2=C.
C IF (M2.EQ.0) GO TO 2
C CALL BDB(1,B,DB,C,C)
C I2=2+(M2-1)*KMAX2
C I3=I2+1
C I4=I3+1
C I2=B*DI*((-1.5*Z(1,I2)+2.*Z(1,I3)-.5*Z(1,I4))/DEL+.5*SOE*BET)
C C1=.5*PHEE*T2
C *****
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BX1(M2)=BET
BT1(M2)=-BET
EX1(M2)=-BET
ET1(M1)=Q1
IF(M3.EQ.0) GO TO 2
EXX1(M3)=Q1
ETX1(M3)=-Q1
TC=0
2 IF(M0.EQ.0) GO TO 3
EX1(M0)=BET
BT1(M0)=BET
CALL BOB(1,8,DB,D,CC)
CALL TLCD(1,2)
I2=2+(M0-1)*KMAX2
I3=I2+1
I4=I3+1
TC=B*SI*((-1.5*Z(1,I2)+2.*Z(1,I3)-.5*Z(1,I4))/DEL+CMXI(1)*Z(3,I2)
1+.5*SOE*BET)-TT(M0)*ALCD
3 EXX1(M1)=PTEE*(T0+.5*T2)
ETX1(M1)=PTEE*(T0+.5*T2)
1CCC CCNTINUE
PTEE=(1.5*Z(3,I2)-2.*Z(3,I3)+.5*Z(3,I4))/DEL+CMXI(1)*Z(1,I2)
T2=C
IF(M2.EQ.0) GO TO 1002
CALL BOB(1,8,DB,D,CC)
I2=2+(M2-1)*KMAX2
I3=I2+1
I4=I3+1
PFX1=PHIXB(KMAX+1)
PFX2=PHIXB(2*KMAX+1)
PFX1=(1.5*Z(3,I2-KMAX2)-2.*Z(3,I3-KMAX2)+.5*Z(3,I4-KMAX2))/DEL+
1CMXI(1)*Z(1,I2-KMAX2)
EX1(M2)=.5*(PTEE*(PTEE+2.*PFX1)-PTEN*(PHEN+2.*PHX2))
IF(ITRMAX.EQ.1) BX1(M2)=0.
BT1(M2)=-BX1(M2)
T2=B*DI*((-1.5*Z(1,I2)+2.*Z(1,I3)-.5*Z(1,I4))/DEL+.5*SOE*BX1(M2))
EX1(M2)=-BX1(M2)
T2=B*DI*((-1.5*Z(1,I2)+2.*Z(1,I3)-.5*Z(1,I4))/DEL+.5*SOE*BX1(M2))
M2L=M2-1
EX1(M2L)=PTEE*(PTEN+PHX2)+PHX1*PTEN
IF(ITRMAX.EQ.1) BX1(M2L)=0.
BT1(M2L)=-BX1(M2L)
EX1(M2L)=BX1(M2L)
T2A=B*DI*((-1.5*Z(1,I2-KMAX2)+2.*Z(1,I3-KMAX2)-.5*Z(1,I4-KMAX2))
1/DEL+.5*SOE*BX1(M2L))
1002 TC=C
IF(M0.EQ.0) GO TO 1003
EX1(M0)=.5*(PTEE*(PTEE+2.*PHX1)+PTEN*(PHEN+2.*PHX2))
IF(ITRMAX.EQ.1) BX1(M0)=0.

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C** P-HAT MATRICES FOR EACH MEDICIAN STATION K AND FOURIER MCDE MN**00008400
C** THESE MATRICES ARE COMPUTED AND SAVED BECAUSE THEY DC NCT **C0008410
C** CHANGE DURING EITHER THE ITERATION PROCEDURE OR THE LOAC INCRE- **C0008420
C** MENT PROCEDURE - AS THEY ARE A FUNCTION OF THE SPELL'S INITIAL **00008430
C** GEOMETRY AND STIFFNESS. **00008440
C** **00008450
C** DIMENSION P(4,4,1), CEE(4,4,1), DST(4,4,1), X(4,1) **00008460
C** COMMON /IBL4/ KMAX, KL BEE(4,4), C(4,4,99), **00008470
C** COMMON /IBL1/ A(4,4), ZF4M(4,4,99) **00008480
C** COMMON /IBL4/ ZF3M(4,4,99), IPIVOT(4), INDEX(4,2), X2(4) **0008510
C** DIMENSION TM(4,4), **0008520
C** INKL=K+KMAX*(MN-1) **0008530
C** IKL=IKL-1 **0008540
C** DO 1 I=1,4 **0008550
C** DO 1 J=1,4 **0008560
C** SUM=0. **0008570
C** DO 2 L=1,4 **0008580
C** SUM=SUM+C(I,L)*P(L,J,KL) **0008590
C** TM(I,J)=BEE(I,J)-SUM **0008600
C** CALL MATINV(TM,4,X2,0,DETERM,IPIVOT,INDEX,4,ISCALE) **0008610
C** DO 5 I=1,4 **0008620
C** DO 5 J=1,4 **0008630
C** SUMA=0. **0008640
C** DO 6 L=1,4 **0008650
C** SUMA=SUMA+TM(I,L)*A(L,J) **0008660
C** SUMC=SUMC+TM(I,L)*C(L,J) **0008670
C** P(I,J,IKL)=SUMA **0008680
C** DEE(I,J,IKL)=TM(I,J) **0008690
C** DST(I,J,IKL)=SUMC **0008700
C** RETURN **0008710
C** ENDC **0008720
C** SUBROUTINE HNLPOL(Z,PHIXB,PHITB) **0008730
C** **0008740
C** THIS SUBROUTINE COMPUTES THE NON-LINEAR TERMS BETA-SUB S **0008750
C** -SUB THETA, -SUB S-THETA, ETA-SUB S-S, AND -SUB THETA-S AT A **0008760
C** FINAL PCLE. **0008770
C** **0008780
C** DIMENSION Z(4,1), PHIXB(1), PHITB(1) **0008790
C** COMMON /IBL1/ MNMAX **0008800
C** COMMON /IBL3/ M0,M1,M2,M3 **0008810
C** COMMON /IBL4/ KMAX, KL **0008820
C** COMMON /IBL12/ KMAX1,KMAX2,NCONV **0008830
C** COMMON /IBL13/ ITRMAX,LSMAX **0008840
C** COMMON /IBLJ/ JUMP **0008850
C** COMMON /IBL5/ TT(99),EMT(99),DT(59),DMT(99) **0008860
C** **0008870

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IC=B*SI*((1.5*Z(1,KM)-2.*Z(1,KM1))+.5*Z(1,KM2))/DEL+CMXI(KMAX)*
1Z(3,KM)+.5*SOE*BE1)-TT(MO)*ALOAD
3EX3(M1)=PHEE*(TO+.5*T2)
RETURN
C*****
10CC CCAI INUE
T2=C.
IF(M2.EQ.0) GO TO 1002
KA=KMAX1+(M2-1)*KMAX2
KA1=KM-1
KA2=KMAX*2
J=J+KMAX
I=J+KMAX
PFX1=PHIXB(J)
PFX2=PHIXB(I)
PFEN=-1.5*Z(3,KM-KMAX2)-2.*Z(3,KM1-KMAX2)+.5*Z(3,KM2-KMAX2))/DEL
1+CMXI(KMAX)*Z(1,KM-KMAX2)
BX3(M2)=.5*(PHEE*(PHEN+2.*PHX2)
IF(ITRMAX.EQ.1) BX3(M2)=0.
BT3(M2)=-BX3(M2)
BX12(M2)=BX3(M2)
M2L=M2-1
BX3(M2L)=PHEE*(PHEN+PHX2)+PFX1*PFEN
IF(ITRMAX.EQ.1) BX3(M2L)=0.
BT3(M2L)=-BX3(M2L)
BX12(M2L)=-BX3(M2L)
T2=B*DI*((1.5*Z(1,KM)-2.*Z(1,KM1))+.5*Z(1,KM2))/DEL+.5*SCE*B*BX3(M2)
T2A=B*DI*((1.5*Z(1,KM-KMAX2)-2.*Z(1,KM1-KMAX2))+.5*Z(1,KM2-KMAX2)
1/DEL+.5*SOE*B*BX3(M2L))
10C2 TC=C.
IF(MO.EQ.0) GO TO 1003
CALL TLCD(KMAX,Z)
KA=KMAX1+(MO-1)*KMAX2
KA1=KM-1
KA2=KM-2
PFX3(MO)=-.5*(PHEE*(PHEE+2.*PHX1)+PFEN*(PHEN+2.*PHX2))
IF(ITRMAX.EQ.1) BX3(MO)=0.
BT3(MO)=BX3(MO)
TC=B*SI*((1.5*Z(1,KM)-2.*Z(1,KM1))+.5*Z(1,KM2))/DEL+CMXI(KMAX)*
1Z(3,KM)+.5*SOE*B*BX3(MO)-TT(MO)*ALOAD
10C3 IF(ITRMAX.EQ.1) GO TO 1001
PFSS=PHEN+PHX2
PFSP=PHEN+PHX2
M1L=M1-1
EX3(M1)=PHSS*TO+.5*(PHSS*T2+PHSP*T2N)
EX3(M1)=PHSP*TO-.5*(PHSP*T2-PHSS*T2N)
ETX3(M1)=.5*(PHSS*T2+PHSP*T2N)
ETX3(M1L)=-.5*(-PHSP*T2+PHSS*T2N)

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00010290
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IF(M3.EQ.0) GO TO 1001
N=L=M3-1
MEXX3(M3)=.5*(PHSS*T2-PHSP*T2N)
EEXX3(M3)=.5*(PHSS*T2N+PHSP*T2)
EEXX3(M3)=.5*(-PHSS*T2+PHSP*T2N)
EEXX3(M3)=.5*(-PHSS*T2-PHSS*T2N)
1001 CONTINUE
RETURN
END
SUBROUTINE PHIBET(K,Z,IS,JS,ID,JD,PHIXB,PHITB)
*****
***** SUBROUTINE CALCULATES THE PHI'S AND CARRIES OUT THE
***** MULTIPLYING AND SUMMATION PROCEDURE FOR COMPUTING THE BETA
***** NON-LINEAR TERMS FOR A GIVEN MERIDIONAL STATION K. THE ARRAYS
***** IS,JS,ID,JS,JS,JS,MAXC,MAXSY ARE PREPARED IN SUB-
***** ROUTINE MCDES AND USED HERE.
*****
***** DIMENSION Z(4,1),IS(99,1),JS(99,1),ID(99,1),JD(99,1),PHIXB(1),
***** PHITB(1)
***** COMMON /IBL1/ MNMAX
***** COMMON /IBL2/ N(99),MNINIT
***** COMMON /IBL4/ KMAX,KL
***** COMMON /IBL7/ MNMAXO,MAXD(99),MAXS(59),MAXSY(59),IJS(59)
***** COMMON /IBL12/ KMAX1,KMAX2,NCONV
***** COMMON /IBL13/ ITRMAX,LSMAX
***** COMMON /IBL13/ JUMP
***** COMMON /IBL6/ SOE,CSE,ALOAD
***** COMMON /IBL8/ R(500),GAM(500),OMT(500)
***** COMMON /IBL10/ PHIX(99),PHIT(99),PHI(99)
***** COMMON /IBL11/ OMXI(500),PHEE,T0,T2
***** COMMON /IBL12/ TDLI,TDEL
***** COMMON /IBL15/ NU,UI(99),V1(99),V2(59),U2(95),W2(59),U3(59),
***** V3(95),W3(99)
***** COMMON /BL27/ BX3(59),BT3(99),BXT2(99),BE3(59)
***** COMMON /BLPHS/ PHX(99),PHI(99)
*****
***** CX=CMXI(K)
***** CT=CMT(K)
***** CTA=1.,Q(K)
***** GA=GAW(K)
***** KP2=K+2
***** CC 1 N=1,MNMAXO
***** EN=N(M)
***** IK=KP2+(M-1)*KMAX2
***** U3(M)=Z(1,IK)
***** V3(M)=Z(2,IK)
***** W3(M)=Z(3,IK)
***** PHIX(M)=Z(4,IK)*W3(M)-W1(M))+CX*U2(M)

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45      BE2(M)=SMF
      CCATINUE
      ENCL
      SLE ROUTINE HJ(K,MN)
      *****
      ***** THIS SUBROUTINE COMPUTES THE ELEMENTS OF THE H AND JAY
      ***** MATRICES FOR BOTH FOUNDARIES OF THE SPELL
      *****
      ***** LSD18, JAY, NU
      *****
      REAL L2, LAM2, LSD1N, MNINIT
      COMMON /BL2/ N(99), MNINIT
      COMMON /BL4/ KMAX, KL
      COMMON /BL8/ R(500), GAM(500), OMT(500)
      COMMON /BL11/ OMTI(500), PHEE, IO, T2
      COMMON /BL14/ LAM2, LSD18, LSD1N
      COMMON /BL15/ NU, UI(99), V1(99), W1(99), V2(99), W2(99), U3(99),
      1 V3(99), W3(99)
      COMMON /BL17/ DEL
      COMMON /BL20/ DEOMX(500)
      COMMON /BL23/ JAY(4,4), H(4,4)
      EQUIVALENCE(L2, LAM2)
      *****
      CALL BCB(K,B,DB,U,DD)
      YAF=1
      IF(K.EQ.1.OR.K.EQ.KMAX)YAH=2,
      C1=(1.-NU)
      GA=GAM(K)
      CX=CMXI(K)
      RA=R(K)
      ENR=EN/RA
      REG=0
      IF(YAF.EQ.2.) REG=1.
      C1=CMT(K)
      CXI=3.*CMXI(K)-OMT(K)
      CTX=3.*CMT(K)-OMXI(K)
      CL=C*L2*D1*ENR
      F(1,1)=B
      F(1,2)=0.
      F(1,3)=0.
      F(1,4)=0.
      F(2,1)=0.
      F(2,2)=B*D1/2.*L2*D1/8.*CTX**2*REG
      F(2,3)=CL/2.*CTX*REG
      F(2,4)=0.
      F(3,1)=0.
      F(3,2)=CL*CTX*YAH/4.
      ENR2=ENR**2

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C*****
N=NM(MASS(K)
N7C=MASS(K)
CALL BCDB(K,B,DB,D,CC)
E(1,2)=C.
E(1,3)=C.
E(1,4)=C.
E(2,1)=C.
C1=R*(1.-NU)
RA=GAM(K)
C1=CMXI(K)
C1=DECMX(K)
LEX=(3.*OT-OT)
REX=GA*2
GAZE=(3.*OX-OT)
C1X=OT*CX
C1NR=LAM2*D*N*D1/(2.*RA)
C1NR=LAM2*DD/D
C1NR=LAM2*D*D1*REX**2/8.
E(2,2)=C.
E(2,3)=C.
E(2,4)=C.
E(3,1)=C.
E(3,2)=E(2,3)
E(3,3)=N/FA**2
E(3,4)=LAM2
E(4,1)=C.
E(4,2)=C.
E(4,3)=C.
E(4,4)=C.
F(1,1)=GA*8+DB
F(1,2)=(1.+NU)*B*N/(2.*RA)+CNLR*REX*RXE/4.
F(1,3)=B*(OX+NU*OT)+LAM2*D*D1*((1.+NU)*GA2*CX+RAN*RXE/2.)
F(1,4)=LAM2*OX
F(2,1)=F(1,2)
F(2,2)=(D1/2.)*(GA*8+DB)-(LAM2*CX*OT*REX/8.)*(2.*DEX-GA*(5.*OX
1-F(2,3)*OT))+LAM2*DD*OT*REX**2/8.
F(2,3)=CNLR*(2.*(1.+NU)*GA*OT-DEX+3.*GA*(CX-CT))+CNLR*REX
F(2,4)=C.
F(3,1)=F(1,3)
F(3,2)=CNLR*(3.*GA*OX-GA*OT*(5.+2.*NU)-DEX)+CNLR*REX
F(3,3)=F(2,3)-LAM2*D*D1*((1.+NU)*GA*OX*OT+GA**3)+2.*GA*RAN)
1+LAM2*CC*D1*((1.+NU)*GA2+2.*RAN)
F(4,1)=LAM2*GA*(2.-NU)
F(4,2)=C*EX

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F(4,2)=0.*NU*GA
F(4,3)=0.*NU*GA
F(4,4)=0.*NU*GA
G(1,1)=NU*DB*GA-NU*B*OTX-B*GA2-C1*B*GAN/2.-LAM2*D*D1*((1.+NU)*GA2*
1CX**2+RXE**2*GAN/8.)
2MAS/DELSO
G(1,2)=NU*DB*GA-NU*B*OTX-B*GA2-C1*B*GAN/2.-LAM2*D*D1*((1.+NU)*GA2*
1+(1.+NU)*OTX)
G(1,3)=B*(DEX+GA*(OX-OT))+DB*(OX+NU*OT)-LAM2*D*D1*GA*GAN*(RXE/2.+(
11.+NU)*OX)
G(1,4)=LAM2*D1*GA*CX
G(2,1)=B*GAN*(3.-NU)/(2.*RA)-D1*NU*DB/(2.*RA)+DNLN*2.*(-1.+(1.+
1NU)*GA*CTX+GA/8.*(6.*OTX-7.*OX**2-3.*OT**2)-DEX/4.*(5.*CT-3.*CX))
1NLCALR/4.*REX*RXE
2-G(2,2)=-GA*REX(2,2)+D1/2.*B*OTX-B*GAN-LAM2*D*D1*((1.+NU)*CT**2*GAN
1-CTX/8.*REX**2)
2MAS/DELSO
G(2,3)=B*GAN*(OT+NU*OX)/RA+DNLN*(GA*DEX-2.*GA2*OX-2.*(1.+NU)*CT
1*GAN+REX*(GA2+OTX))-DNLN*REX*GA
G(2,4)=-NU*LAM2*OT*NU/RA
G(3,1)=-B*GA*(OT+NU*OX)+LAM2*D*D1*(GA*(1.+NL)*(-GA*DEX+GA2*OX
1-CX*GAN+2.*OTX*CX)+GAN/2.*(GA*CX-GA*OT-3.*DEX))
2-LAM2*CC*D1*((1.+NU)*GA2*OX+GAN/2.*RXE)
1G(3,2)=-B*GAN*(OT+NU*CX)/RA+DNLN*(2.*(1.+NU)*OTX*OT-GA2*OX+2.*GA2
1*CT+GA*REX)
2G(3,3)=-B*(OX**2+2.*NU*OTX+OT**2)+LAM2*D*D1*GAN*((1.+NU)*CTX-RAN
1+2.*GA2+CTX))-LAM2*D*D1*GAN*(3.+NL)*GA
2MAS/DELSO
G(3,4)=-LAM2*(D1*CTX+NU*GAN)
G(4,1)=C*(DEX+NU*GA*OX)
G(4,2)=C*(NU*GAN
G(4,3)=C*NU*GAN
G(4,4)=-1.
RETURN
END
SUBROUTINE POLE(K,P,DEE,DST,X,Z,ZC,Z2,Z3,ZDCT,IS,JS,ID,JD,PHIXB,
1PFI,IB)
C*****
C***** THIS SUBROUTINE PRINTS THE SOLUTION AT AN INITIAL AND A FINAL
C***** FCLE.
C*****
1INFLICIT LCGICAL*1 ($)
REAL NU,MT,MX,MTH,MXT,MTS,KX,KT,KXT,LAM,LAM2,MASS
C1PARAMENSION P(4,4,1),DEE(4,4,1),X(4,1),Z(4,1),ZC(4,1),
1Z(4,1),Z3(4,1),ZDCT(4,1),IS(99,1),JS(99,1),ID(99,1),JD(99,1),
2PFI(1),PHI(1),IBL2/N(99),MNINIT
C*****

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CCMMCN /IBL3/ MO,M1,M2,M3
CCMMCN /IBL4/ KMAX,KL,IBCFNL
CCMMCN /IBL5/ IBCINL,MAXD(99),MAXS(59),MAXSY(99),IJS(59)
CCMMCN /IBL7/ MNMAXO,ISTEP,ITR
CCMMCN /IBL8/ LSTEP,NT+MAX
CCMMCN /IBL10/ IFREQ,NT+MAX
CCMMCN /IBL12/ KMAX1,KMAX2,ACGNV
CCMMCN /IBLJ/ JUMP
CCMMCN /BL4/ ZFIM(4,4,59),ZF2M(4,4,99),
1 ZFIM(4,4,59),ZF4M(4,4,99),
CCMMCN /BL5/ TT(99),MT(99),DT(99),DMT(99)
CCMMCN /BL6/ SQE,S1
CCMMCN /BL7/ OL(500),GAM(500),CMT(500)
CCMMCN /BL8/ R(500),PHIX(59),PHIT(99),PHI(99)
CCMMCN /BL10/ OMXI(500),PHEE,I0,T2
CCMMCN /BL11/ PHEN,T2N
CCMMCN /BL11A/ TDLI,TDDEL
CCMMCN /BL12/ LAM2,LSDB,LSDBIN
CCMMCN /BL14/ NU,U1(99),V1(99),W1(99),V2(99),U2(99),W2(99),U3(99),
1 V3(99),W3(99)
CCMMCN /BL17/ DEL
CCMMCN /BL19/ TH(36)
CCMMCN /BL20/ DEOMX(500)
CCMMCN /BL27/ BX3(59),BT3(99),BX13(99),BE3(59)
CCMMCN /BL31/ DELSQ,EXT1(99)
CCMMCN /BL32/ TKN,ELAST,CHAR,SIGC
CCMMCN /BL100/ TEEG,$DYNMC
CCMMCN /BL101/ DELSD
CCMMCN /BL102/ DELCAD
CCMMCN /BL103/ MASS(500)
CCMMCN /BL110/ TX(99),TTH(99),TXT(99),MA(59),MTH(59),MXI(59),
1 QS(99)
CCMMCN /BL111/ ABZ,ABZ0,ABZN,ABZ3,DD2
C*****
CALL BCE(K,BS,DB,CS,DD)
M1L=M1-1
M2L=M2-1
IF(K.EQ.KMAX) GO TO 301
LL(202,MN)=L2(MN)
V1(MN)=V2(MN)
W1(MN)=W2(MN)
I1=I3-1
I2=(MN)=Z(1,I3)
V2(MN)=Z(2,I3)
W2(MN)=Z(3,I3)

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10C2 CCAT INUE
      II=KMAX+(M1-1)*KMAX2
      IF I=II+1
      IF I=II-1
      GAK=GAM(KL)
      CALL TLCD(KL,BS,DB,CS,DD)
      PFIIX=Z(3,II)*TDLI+OMXI(KL)*Z(1,II)
      PFIIT=Z(3,II)/R(KL)*Z(2,II)
      PFI=Z(2,II)*Z(2,II)*TDLI+GAK*Z(2,II)/R(KL))/2.
      CS(M1)=-SIGO*TKN*LCAC-DS*DI*(-PFIIX/R(KL)-GAK*PHIIT+OMXI(KL)-OMXI
      *GAK)+CI*MT(M1)*ALCAC-DS*DI*(-PFIIX/R(KL)-GAK*PHIIT+OMXI(KL)
      (KL))*PHIIT+(-Z(3,II)*TDLI-GAK*Z(3,II))/R(KL)+GAK*(CMXI(KL)
      -OMT(KL))*Z(2,II)+CMT(KL)*(Z(2,II)*Z(2,II)*TDLI)*.5)
      /DEL
      IF(MO.EQ.0) GO TO 304
      TX(MO)=TO*ABZ
      TTH(MO)=TO*ABZ
      TTF(MO)=MX(MO)
      3C4 IF(M2.EQ.0) GO TO 305
      TX(M2)=T2*ABZ
      TTH(M2)=-T2*ABZ
      TTF(M2)=T2*ABZ
      MXT(M2)=-MX(M2)
      IF(JUMP.EQ.1) GO TC 305
      TX(M2L)=T2N*ABZ
      TTH(M2L)=-TX(M2L)
      TTF(M2L)=-TX(M2L)
      MXT(M2L)=-MX(M2L)
      GC TO 305
      3C3 IF(MO.EQ.0) GO TO 306
      IKM=KMAX+(MO-1)*KMAX2
      IM1=IKM-1
      TX(MO)=BS*SI*(-2.*Z(1,IKM)+.5*Z(1,IM1))/CEL+CMXI(KMAX)*Z(3,IKM+1)
      1 CALL TLCD(KMAX,Z)
      TX(MO)=BS*ABZ-TT(MO)*ABZ*ALCAD
      TTF(MO)=TX(MO)
      TTH(MO)=MX(MO)
      3C6 IF(M2.EQ.0) GO TO 305
      IKM=KMAX+(M2-1)*KMAX2
      IM1=IKM-1
      TX(M2)=BS*DI*(-2.*Z(1,IKM)+.5*Z(1,IM1))/DEL
      TTH(M2)=TX(M2)*ABZ
      TTF(M2)=-TX(M2)
      MXT(M2)=-MX(M2)

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C *** SET UP THIRD LOOP - TC COMPARE SUM WITH ALL OTHER MCDES *** 00018480
C *** 302 MMFT=1, MNMAX, JUMP *** 00018490
C *** IF WE SATISFY HERE, MODE EXISTS, GC TO INCREMENT -MAXS- CR *** 00018500
C *** -MAXSY- *** 00018510
C *** IF (ICORFL.EQ.1) GC TO 301 *** 00018520
C *** IF (MNMAX.GE.MAXM) GC TO 301 *** 00018530
C *** IF (ICORFL.EQ.1) GC TO 301 *** 00018540
C *** IF (MNMAX.GE.MAXM) GC TO 301 *** 00018550
C *** IF WE MAKE IT TO HERE, WE HAVE GENERATED A NEW MODE *** 00018560
C *** IF WE WANT ANY MORE NEW MODES *** 00018570
C *** IF (ICORFL.EQ.1) GC TO 301 *** 00018580
C *** IF (MNMAX.GE.MAXM) GC TO 301 *** 00018590
C *** INCREMENT -MNMAX- AND ESTABLISH NEW MODE NUMBER *** 00018600
C *** MNMAX=MNMAX+JUMP *** 00018610
C *** N(MNMAX)=NTEST *** 00018620
C *** IF (JUMP.GT.1) N(MNMAX-1)=-NTEST *** 00018630
C *** IF (MNMAX.GE.MAXM) ICORFL=1 *** 00018640
C *** IF MCDE WAS ADDED TO ITSELF, GO TO -MAXSY AND IJS- SECTION *** 00018650
C *** 31C IF (MNMAX.EQ.NMM) GC TO 360 *** 00018660
C *** MAKE ENTRIES IN -LOCS-, -IS- AND -JS- *** 00018670
C *** LCCS=MAXS(MMFT)+1 *** 00018680
C *** MAXS(MMFT)=LOCS *** 00018690
C *** JS(LOCS,MMFT)=MM *** 00018700
C *** GC TO 301 *** 00018710
C *** SEE IF THE SUM OF THE MCDE WITH ITSELF WAS THE 0-TH MCDE *** 00018720
C *** 36C IF (MMN.EQ.C) GO TO 301 *** 00018730
C *** IF HERE, IT WASN'T, MAKE ENTRIES IN -MAXSY- AND -IJS- *** 00018740
C *** MAXSY(MMFT)=1 *** 00018750
C *** IJS(MMFT)=MN *** 00018760
C *** 3C1 CONTINUE *** 00018770
C *** MNINIT=MNMAXG+JUMP *** 00018780
C *** IF (ICORFL.GT.0) IPASS=IPASS+1 *** 00018790
C *** *** 00018800
C *** *** 00018810
C *** *** 00018820
C *** *** 00018830
C *** *** 00018840
C *** *** 00018850
C *** *** 00018860
C *** *** 00018870
C *** *** 00018880
C *** *** 00018890
C *** *** 00018900
C *** *** 00018910
C *** *** 00018920
C *** *** 00018930
C *** *** 00018940
C *** *** 00018950

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IF(IPASS.LT.2.AND.MNINIT.LE.MNMAX) CALL PMATRX (P,X,ZC,Z2,Z3,CEE,
1DST)
IF(RETUR)
ENL
ROUTINE TEAETA(K,Z,IS,JS,ID,JC)
C*****
C THIS SUBROUTINE CALCULATES THE INPLANE FORCES AND CARRIES CUT
C THE MULTIPLYING AND SUMMATION FOR COMPUTING THE ETA
C ACN-LINEAR TERMS FOR A GIVEN MERIDIONAL STATION K. THE ARRAYS
C IS,JS,ID,JS,MAXS,MAXC,MAXSY PREPARED IN SUBROUTINE
C MODES ARE USED HERE
C*****
REAL NU,MT
DIMENSION Z(4,1),IS(99,1),JS(99,1),ID(99,1),JC(99,1)
COMMON /IBL1/ MNMAX
COMMON /IBL2/ N(99),MNINIT
COMMON /IBL7/ MNMAXO,MAXD(99),MAXS(99),MAXSY(99),IJS(99)
COMMON /IBL8/ LSTEP,ITR
COMMON /IBL13/ ITRMAX,LSMAX
5/IBLJ/ JUMP
COMMON /BL5/ TT(99),MT(99),DT(99),DMT(99)
COMMON /BL6/ SOE,CSE,ALOAD
COMMON /BL7/ DL,SCC,SI
COMMON /BL8/ R(500),GAM(500),OMT(500)
COMMON /BL10/ PHIX(99),PHT(99),PHI(99)
COMMON /BL11/ OMXI(500),PHEE,T0,T2
COMMON /BL12/ TDLI,TDEL
COMMON /BL15/ NU,UI(99),V1(99),V2(99),U2(99),U3(99),
1 CCMMGN /BL27/ BX3(99),BT3(99),BXI2(99),BE2(99)
COMMON /BL28/ EXX3(99),ETT3(99),ETX3(99),EX3(99),ET3(99)
COMMON /BLPHS/ PHX(99),PHT(99)
C*****
C DIMENSION ICN*****
C RRA=1./R(K)
C GA=GAM(K)
C X=CMXI(K)
C T=CMT(K)
C CALL BCE(K,BS,DB,CS,DD)
C I=1,MNMAXO
C FIX(M)=PHIX(M)+PHX(M)
C PHT(M)=PHT(M)+PHT(M)
C EN=N(M)
C CALL TLGAD(K,Z)
C TTS=TT(M)+ALQAD
C EX=(U3(M)-UI(M))*TDLI+OX*W2(M)+CSE*(BX3(M)+EE3(M))
C ET=EN #V2(M)*RRA+GA*U2(M)+OT*W2(M)+DSE*(ET2(M)+BE3(M))
C EXT=.5*(TDLI*(V3(M)-V1(M))-EN #U2(M)*RRA-GA*V2(M))+CSE*EXT3(M)
000189560
000189570
000189580
000189590
000190000
000190010
000190020
000190030
000190040
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000190060
000190070
000190080
000190090
000190100
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00019910

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TX(N)=BS*(EX+NU*EI)-TTS
TTH(M)=BS*(ET+NU*EX)-TTS
TXT(M)=BS*CI*EXT
1 IF(JUMP.EQ.2) GO TC 1111
CC 9 N=1,MNMAX
SMF=0.
SMV=0.
SME=0.
SMN=0.
SMT=0.
IF(N(M).EQ.0) GO TC 20
IF(MXL=MAXS(N))
IF(MXL.EQ.0) GO TO 2
CC 3 L=1,MAXL
I=JS(L,M)
J=JF=SMF+TX(I)*PHIX(J)+TTH(J)*PHIX(I)
K=KS=SMV+TTH(I)*PHIT(J)-PHIT(J)*TTH(I)
L=LS=SMV+PHIX(I)*TTH(J)+PHIX(J)*TTH(I)
M=MS=SMV+PHIX(I)*PHI(J)+TX(J)*PHI(I)
N=NS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
O=OS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
P=PS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
Q=QS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
R=RS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
S=SS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
T=TS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
U=US=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
V=VS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
W=WS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
X=XS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
Y=YS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
Z=ZS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
3 IF(MXL.EQ.0) GO TO 4
CC 5 L=1,MAXL
I=JS(L,M)
J=JF=SMF+TX(I)*PHIX(J)+TTH(J)*PHIX(I)
K=KS=SMV+TTH(I)*PHIT(J)+PHIT(J)*TTH(I)
L=LS=SMV+PHIX(I)*TTH(J)+PHIX(J)*TTH(I)
M=MS=SMV+PHIX(I)*PHI(J)+TX(J)*PHI(I)
N=NS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
O=OS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
P=PS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
Q=QS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
R=RS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
S=SS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
T=TS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
U=US=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
V=VS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
W=WS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
X=XS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
Y=YS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
Z=ZS=SMN+TTH(I)*PHI(J)+TTH(J)*PHI(I)
5 IF(MXL.EQ.0) GO TC 10
CC 7 L=1,MNMAX
I=JS(L,M)
J=JF=SMF+TX(I)*PHIX(I)
K=KS=SMV+TTH(I)*PHIT(I)
L=LS=SMV+PHIX(I)*TTH(I)
M=MS=SMV+PHIX(I)*PHI(I)
N=NS=SMN+TTH(I)*PHI(I)
O=OS=SMN+TTH(I)*PHI(I)
P=PS=SMN+TTH(I)*PHI(I)
Q=QS=SMN+TTH(I)*PHI(I)
R=RS=SMN+TTH(I)*PHI(I)
S=SS=SMN+TTH(I)*PHI(I)
T=TS=SMN+TTH(I)*PHI(I)
U=US=SMN+TTH(I)*PHI(I)
V=VS=SMN+TTH(I)*PHI(I)
W=WS=SMN+TTH(I)*PHI(I)
X=XS=SMN+TTH(I)*PHI(I)
Y=YS=SMN+TTH(I)*PHI(I)
Z=ZS=SMN+TTH(I)*PHI(I)
20 CC 21 L=1,MNMAX
I=JS(L,M)
J=JF=SMF+TX(L)*PHIX(L)
K=KS=SMV+PHIT(L)*TTH(L)
L=LS=SMV+PHIX(L)*PHI(L)
M=MS=SMN+TTH(L)*PHI(L)
N=NS=SMN+TTH(L)*PHI(L)
O=OS=SMN+TTH(L)*PHI(L)
P=PS=SMN+TTH(L)*PHI(L)
Q=QS=SMN+TTH(L)*PHI(L)
R=RS=SMN+TTH(L)*PHI(L)
S=SS=SMN+TTH(L)*PHI(L)
T=TS=SMN+TTH(L)*PHI(L)
U=US=SMN+TTH(L)*PHI(L)
V=VS=SMN+TTH(L)*PHI(L)
W=WS=SMN+TTH(L)*PHI(L)
X=XS=SMN+TTH(L)*PHI(L)
Y=YS=SMN+TTH(L)*PHI(L)
Z=ZS=SMN+TTH(L)*PHI(L)
21 IF(M.GT.MNMAXO) GO TO 10
SMF=SMF+TX(M)*PHIX(M)

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00019930
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00020280
00020290
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00020340
00020350
00020360
00020370
00020380
00020390

1C EXX3(M)=SMF*.5
  ETX3(M)=SMV*.5
  EXX3(M)=SMV*.5
  ETX3(M)=SMV*.5
  S CC(NT)INUE
  CC TO 2222
*****
C THIS SECTION HANDLES GENERAL LOADING
C
C *****
C 1111 CC 45 N=1, NMAX
C SMF=0.0
C SMV=0.0
C SME=0.0
C SMT=0.0
C *****
C TEST FOR ASYMMETRIC MCDE
C *****
C IF (N(M)-LT.0) GO TO 101
C *****
C THIS SECTION HANDLES SYMMETRIC COMBINATIONS
C *****
C TEST FOR ZERO-TH MCDE
C *****
C IF (N(M).EQ.0) GO TO 420
C PAXL=MAXS(N)
C *****
C TEST FOR PRESENCE OF SYMMETRIC SLMMATION COMBINATIONS
C *****
C IF (MAXL.EQ.0) GO TO 42
C *****
C SET UP COUPLING MODES- INDICES AND TEST FOR MCDE 1
C *****
C 43 L=1, MAXL
C JS(L,M)
C JS(L,M)
C I=I-1
C J=J-1
C IF (I.EC.1) GO TO 43

```





```

C** 101 MF=M+1
C** MAXL=MAXS(MP)
C** TEST FOR PRESENCE OF SUMMATION COMBINATIONS
C** IF (MAXL.EQ.0) GO TO 102
C** SET UP COUPLING INDICES AND TEST FOR MODE 1
C** DC 103 L=1,MAXL
C** I=JS(L,MP)
C** J=J-I-1
C** IF (I.EQ.1) GO TO 103
C** CCPILE SUMS FOR ASYMMETRIC SUMMATION COMBINATIONS
C** SMF=SMF+PHIX(I)*TX(JJ)+PHIX(J)*TX(I)+PHIX(I)*TX(J)
C** 1 SPAS=SMS-PHIT(I)*TTH(JJ)-PHIT(J)*TTH(I)+PHIT(I)*TTH(J)
C** 1 SPV=SMV+PHIT(I)*TX(JJ)+PHIT(J)*TX(I)+PHIT(I)*TX(J)
C** 1 SPE=SME+PHIX(I)*TX(JJ)+PHIX(J)*TX(I)-PHIX(I)*TX(J)
C** 1 SNA=SMN-PHI(I)*TX(JJ)-PHI(J)*TX(I)+PHI(I)*TX(J)
C** 1 SNT=SMT-PHI(I)*TTH(JJ)-PHI(J)*TTH(I)+PHI(I)*TTH(J)
C** 1 CCATINUE
C** TEST FOR PRESENCE OF DIFFERENCE COMBINATIONS
C** 102 MAXL=MAXD(MP)
C** IF (MAXL.EQ.0) GO TO 104
C** SET UP COUPLING MGDES- INDICES AND TEST FOR MCDE 1
C** DC 105 L=1,MAXL
C** I=JS(L,MP)
C** J=J-I-1
C** IF (J.EC.1) GO TO 123

```

```

C ***** CCNFILE SUMS FOR ASYMMETRIC DIFFERENCE COMBINATIONS *****
C SMF=SMF-PHIX(I)*TX(JJ)+PHIX(J)*TX(II)+PHIX(II)*TX(J) *****
C 1 SMF=SMF-PHIX(JJ)*TX(I) *****
C 1 SMS=SMS+PHIT(I)*TTH(JJ)+PHIT(J)*TTH(II)+PHIT(II)*TTH(J) *****
C 1 SPV=SPV+PHIT(I)*TTH(JJ)+PHIT(J)*TTH(II)+PHIT(II)*TTH(J) *****
C 1 SME=SME+PHIX(I)*TX(JJ)+PHIX(J)*TX(II)+PHIX(II)*TX(J) *****
C 1 SPN=SPN+PHI(I)*TX(JJ)+PHI(J)*TX(II)+PHI(II)*TX(J) *****
C 1 SMT=SMT+PHI(I)*TTH(JJ)+PHI(J)*TTH(II)+PHI(II)*TTH(J) *****
C 1 GC TO IC5 *****
C ***** EXECUTE BELOW IF J=1 IN DIFF-COMB (OR I=1 IN SUM-COMB) *****
C 123 SMF=SMF+(PHIX(I)*TX(II)+PHIX(II)*TX(I))*2.0 *****
C SMV=SMV+(PHIT(I)*TTH(II)+PHIT(II)*TTH(I))*2.0 *****
C SME=SME+(PHIX(I)*TX(II)+PHIX(II)*TX(I))*2.0 *****
C SPN=SPN+(PHI(I)*TTH(II)+PHI(II)*TTH(I))*2.0 *****
C SMT=SMT+(PHI(I)*TTH(II)+PHI(II)*TTH(I))*2.0 *****
C ***** CCNFILE SUMS FOR ASYMMETRIC DIFFERENCE COMBINATIONS *****
C ***** TEXT FOR PRESENCE OF SAME-INDEX COMBINATIONS *****
C 1C4 IF (MAXSY(MP).EQ.0) GC TO 410 *****
C ***** SET UP COUPLING MCCES- INDICES AND COMPILE SUMS *****
C ***** I=1 JS(MP) *****
C ***** I=1 I *****
C SMF=SMF+PHIX(I)*TX(II)+PHIX(II)*TX(I) *****
C SMV=SMV+PHIT(I)*TTH(II)+PHIT(II)*TTH(I) *****
C SPV=SPV+PHIX(I)*TX(II)+PHIX(II)*TX(I) *****
C SPN=SPN+PHI(I)*TTH(II)+PHI(II)*TTH(I) *****
C SMT=SMT+PHI(I)*TTH(II)+PHI(II)*TTH(I) *****
C ***** CCNFILE SUMS FOR ASYMMETRIC DIFFERENCE COMBINATIONS *****
C ***** PREP+RE -AETA- TERMS *****
C ***** EXTE3(M)=SMF*0.5 *****
C ***** EXTE3(M)=SMV*0.5 *****
C ***** EXTE3(M)=SPN*0.5 *****
C ***** EXTE3(M)=SMT*0.5 *****

```







APPENDIX B

LISTING OF OUTPUT FROM EXAMPLE PROBLEM



[illegible]

104 INITIAL CONDITIONS FOR N° 0 FOLLOW

STATION	U	V	W	S
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

STATION	U	V	W	S	ROT
1	0.0	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0	0.0

THE INITIAL CONDITIONS FOR N-1 EQUATIONS

STATION	U	V	W	M S
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

STATION	U	V	W	M S
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

THE INITIAL CONDITIONS FOR 3-2-10102

STATION	U	V	W	S
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

STATION	U	V	W	S
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

144 INITIAL CONDITIONS FOR R= 4 FOLLOW

STATION	U	V	W	5
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

STATION	U	V	W	5
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0



THE TIME STEP NUMBER IS 250 THE TIME IS 4.5E-03 0.0001-03 SECONDS THE SECTION CIRCUMFERENCE IS 2 ITERATIONS

THE SUMMED FORCES, MOMENTS, DISPLACEMENTS AND ROTATIONS FOLLOW FOR THETA = 0.0

STATION	N S	N THETA	M SUMMA	U S	M S	M THETA	P SUMMA
1	-0.3459E-04	-0.0471E-03	0.0	-0.2172E-04	0.2398E-03	0.5424E-02	0.0
14	0.7020E-04	0.251E-04	0.0	-0.2591E-04	0.2098E-04	0.2424E-02	0.0
27	0.308E-04	-0.224E-04	0.0	-0.2160E-04	-0.615E-04	-0.121E-02	0.0
31	0.2031E-04	0.7875E-03	0.0	0.1122E-04	-0.0755E-02	-0.2740E-02	0.0

STATION	U	V	W	PHI S	PHI THETA	PHI
---------	---	---	---	-------	-----------	-----

1	0.0	0.0	0.2749E-09	0.1778E-09	0.0	0.0
14	-0.6017E-02	0.0	0.1312E-00	-0.3565E-01	0.0	0.0
27	-0.4079E-02	0.0	0.3027E-01	0.5691E-01	0.0	0.0
31	-0.1578E-00	0.0	-0.6352E-10	0.5080E-09	0.0	0.0

THE SUMMED FORCES, MOMENTS, DISPLACEMENTS AND ROTATIONS FOLLOW FOR THETA = 0.161501 CL

STATION	N S	N THETA	M SUMMA	U S	M S	M THETA	P SUMMA
1	0.4580E-04	-0.1275E-04	-0.3960E-02	-0.1034E-04	0.1454E-04	0.6455E-03	-0.1914E-03
14	-0.4554E-04	-0.1291E-05	-0.1549E-02	-0.2561E-04	-0.0858E-03	-0.2420E-03	0.1056E-03
27	-0.3588E-04	-0.6111E-04	0.4616E-02	0.3630E-04	0.2828E-03	0.1065E-03	-0.7260E-04
31	-0.1638E-04	-0.5050E-03	0.3203E-02	0.5690E-04	0.1458E-04	0.6284E-03	0.1160E-04

STATION	U	V	W	PHI S	PHI THETA	PHI
---------	---	---	---	-------	-----------	-----

1	0.0	0.0	-0.6915E-09	0.4816E-08	0.1078E-15	-0.2664E-08
14	0.523E-02	-0.1005E-07	-0.2074E-00	0.2520E-01	0.1778E-15	-0.2797E-08
27	0.2689E-02	-0.1181E-07	-0.4000E-01	-0.3330E-01	0.4164E-08	0.4164E-08
31	0.3275E-10	-0.4139E-15	-0.3176E-10	0.2660E-09	-0.6097E-14	0.2155E-08

APPENDIX C

INPUT DATA GUIDE FOR SATANS-IIA

# INPUT DATA GUIDE FOR SATANS-I, SATANS-II, AND SATANS-IIA

CARD	COLUMNS	FORMAT	ITEM	EXAMPLE	MEANING
1	1-72	18A4	TITLE	-	ENTER ANY 72 CHARACTERS
2	1-5	I5	NO	1	THE PROBLEM NUMBER, 0<N<10000.
2	6-10	L5	\$DYNAMC	F T	FOR A STATIC ANALYSIS, SET \$DYNAMC = F. FOR A DYNAMIC ANALYSIS, SET \$DYNAMC = T.
2	11-15	I5	IMODE	0 1	FOR NO MODAL OUTPUT DATA FOR MODAL OUTPUT DATA.
2	16-20	I5	NDIMEN	0 1	DIMENSIONAL OUTPUT DATA. NONDIMENSIONAL OUTPUT.
2	21-25	I5	NTHMAX	8	SUMMED SOLUTION WILL BE PRINTED AT NTHMAX MERID- IANS, 0<NTHMAX<=36.
2	26-30	I5	IFREQ	2	SOLUTION WILL BE PRINTED AT THE FIRST STATION, EVERY SUBSEQUENT IFREQ STATION AND THE LAST STATION, 0<IFREQ<=KMAX.
2	31-35	I5	IPRINT	3	EVERY IPRINT CONVERGED SOLUTION WILL BE PRINT- ED.
2	36-40	I5	IBCINL	-1 0	IF THE SHELL HAS A POLE AT THE FIRST STATION. IF THE SHELL HAS NO POLE AT THE FIRST STATION.
2	41-45	I5	IBCFNL	-1 0	IF THE SHELL HAS A POLE AT THE LAST STATION. IF THE SHELL HAS NO POLE AT THE LAST STATION.

CARD	COLUMNS	FORMAT	ITEM	EXAMPLE	MEANING
2	46-50	I5	KMAX	35	NUMBER OF MERIDIONAL STATIONS. NOTE: KMAX<201 FOR SATANS -I WITHOUT PLCTS AND KMAX<101 FOR SATANS-I WITH PLOTS OR FOR SATANS -II. SATANS-IIA IS UNLIMITED.
2	51-55	I5	MNMAX	7	NUMBER OF SERIES COEFFICIENTS USED TO DESCRIBE THE INITIAL CONDITIONS, PRESSURE AND THERMAL LOADS (AND INITIAL IMPERFECTIONS IF USING SATANS -II OR IIA). MNMAX<=MAXM.
2	56-60	I5	MAXM	7	MAX NUMBER OF HARMONICS IN THE SOLUTION, LIMITED TO 99.
2	61-65	I5	LSMAX	1 99 3000	FOR A LINEAR ANALYSIS. USE MANY LOAD STEPS FOR A NONLINEAR STATIC ANALYSIS. FOR A DYNAMIC ANALYSIS, LSMAX IS THE NUMBER OF TIME INCREMENTS, WHERE $LSMAX = T_{MAX}/\Delta T$ .
2	66-70	I5	LCHMAX	2 0	THE NUMBER OF LOAD STEP SIZE REDUCTIONS IN A STATIC ANALYSIS, RECOMMENDED RANGE = 2-4. FOR A DYNAMIC ANALYSIS.
2	71-75	I5	ITRMAX	1 30	FOR A LINEAR ANALYSIS. THE NUMBER OF ITERATIONS AT A LOAD OR TIME STEP. FOR A NONLINEAR ANALYSIS, SUGGESTED RANGE = 10-30, UP TO 50 FOR SPECIAL CASES.
2	76-80	I5	IC	0 1	INITIAL CONDITIONS. SET TO 0 FOR A STATIC ANALYSIS, OR FOR A DYNAMIC ANALYSIS WHERE THE SPILL IS AT REST AT $t=0$ . FOR A DYNAMIC ANALYSIS WITH INITIAL CONDITIONS.

CARD	COLUMNS	FORMAT	ITEM	EXAMPLE	MEANING
3	1-12	E12.3	NU	0.3	POISSON'S RATIO, $\nu$ .
3	12-24	E12.3	SIG0	1000.0 1.0	REFERENCE STRESS LEVEL, IF THE INPUT DATA IS DIMENSIONAL.
3	24-36	E12.3	ELAST	.3E8 1.0	REFERENCE MODULUS OF ELASTICITY, $E$ . IF THE INPUT DATA IS DIMENSIONAL.
3	37-48	E12.3	TKN	.4E-2 1.0	REFERENCE THICKNESS, $h$ . IF THE INPUT DATA IS DIMENSIONAL.
3	49-60	E12.3	CHAR	8.16 1.0	CHARACTERISTIC SHELL DIMENSION, $a$ . IF THE INPUT DATA IS DIMENSIONAL.
3	61-72	E12.3	TEED	0.0 .996E-5	IF A STATIC ANALYSIS. REFERENCE TIME, $T_0$ .
<hr/>					
4	1-12	E12.3	DELOAD	0.2      .1823E-6	FOR A STATIC ANALYSIS, DELOAD IS THE LOAD INCRE- MENT. IT REMAINS UN- CHANGED UNTIL THE SOLU- TION FAILS TO CONVERGE IN ITERMAX ITERATIONS, WHEN IT IS REDUCED BY A FACTOR OF FIVE. A MAXIMUM OF LCHMAX SUCH REDUCTIONS WILL OCCUR. FOR A DYNAMIC ANALYSIS, DELOAD IS THE NONDIMEN- SIONAL TIME INCREMENT.
4	13-24	E12.3	EPS	0.01	THE CONVERGENCE CRITERION RECOMMENDED RANGE OF 0.01<EPS<0.001.
<hr/>					
CARD 4A IS ONLY INCLUDED FOR A SATANS-II OR SATANS-IIA RUN.					
4A	1-5	I5	JUMP	1 2	FOR AN ANALYSIS USING SINGLE SERIES EXPANSIONS. FOR AN ANALYSIS USING DOUBLE SERIES EXPANSIONS.
4A	5-10	I5	MPERFS	0 1	AN ANALYSIS WITHOUT IM- PERFECTIONS. AN ANALYSIS WITH IMPERFEC- TIONS. NOTE: IF JUMP=28 MPERFS MAY BE 0 OR 1. IF JUMP =1, MPERFS MUST BE 0. IF MPERFS=1, JUMP MUST BE 2.

---

CARD COLUMN FORMAT ITEM EXAMPLE MEANING

INCLUDE AS MANY CARDS 5 AS NECESSARY TO SPECIFY NTHMAX MERIDIANS. IF NTHMAX EQUALS 0, OMIT CARD 5.

5	1-72	6E12.3	10.0	A LIST OF CIRCUMFERENTIAL COORDINATES $\Theta$ , IN DEGREES AND TENTHS, WHERE THE SOLUTION PRINTOUT IS DESIRED. THE LIST MUST HAVE NTHMAX ENTRIES.
---	------	--------	------	--

---

IF IBCINL = -1, OMIT CARDS 6 THROUGH 14. IF IBCFNL = -1, OMIT CARDS 15 THROUGH 23. CARDS 6 THROUGH 23 DESCRIBE THE BOUNDARY CONDITIONS AT THE FIRST, AND THEN AT THE LAST STATION. THE BOUNDARY CONDITIONS EXIST ON THE TOTAL VARIABLES, NOT ON THE INDIVIDUAL HARMONICS. LOADINGS APPLIED THROUGH SPECIFICATION OF BOUNDARY CONDITIONS ARE TAKEN IN THE ZERO-ETH HARMONIC (N=0) ONLY, AS THE COLUMN MATRIX  $\{1\}$  IS SET TO ZERO FOR HARMONICS GREATER THAN ZERO. THE BOUNDARY CONDITIONS ARE DIMENSIONAL. THE FORMAT OF CARDS 6 THROUGH 23 IS 4E16.8.

CARD 6,15 CARD 7,16 CARD 8,17 CARD 9,18

$$\begin{bmatrix} \Omega(1,1) \\ \Omega(2,1) \\ \Omega(3,1) \\ \Omega(4,1) \end{bmatrix} \begin{bmatrix} \Omega(1,2) \\ \Omega(2,2) \\ \Omega(3,2) \\ \Omega(4,2) \end{bmatrix} \begin{bmatrix} \Omega(1,3) \\ \Omega(2,3) \\ \Omega(3,3) \\ \Omega(4,3) \end{bmatrix} \begin{bmatrix} \Omega(1,4) \\ \Omega(2,4) \\ \Omega(3,4) \\ \Omega(4,4) \end{bmatrix} \begin{bmatrix} N_s \\ N_{s0} \\ Q_s \\ \delta_s \end{bmatrix} +$$

$$\begin{bmatrix} \Lambda(1,1) \\ \Lambda(2,1) \\ \Lambda(3,1) \\ \Lambda(4,1) \end{bmatrix} \begin{bmatrix} \Lambda(1,2) \\ \Lambda(2,2) \\ \Lambda(3,2) \\ \Lambda(4,2) \end{bmatrix} \begin{bmatrix} \Lambda(1,3) \\ \Lambda(2,3) \\ \Lambda(3,3) \\ \Lambda(4,3) \end{bmatrix} \begin{bmatrix} \Lambda(1,4) \\ \Lambda(2,4) \\ \Lambda(3,4) \\ \Lambda(4,4) \end{bmatrix} \begin{bmatrix} U \\ V \\ W \\ M_s \end{bmatrix} = \begin{bmatrix} \lambda(1) \\ \lambda(2) \\ \lambda(3) \\ \lambda(4) \end{bmatrix} \quad \text{CARD 14,23}$$


---

CARD 24 IS:

1. INCLUDED FOR A SATANS-I STATIC ANALYSIS.
2. INCLUDED BUT BLANK FOR A SATANS-I DYNAMIC ANALYSIS.
3. OMITTED FOR A SATANS-II ANALYSIS.
4. INCLUDED BLANK FOR DYNAMIC USED FOR STATIC SATANS-IIA ANALYSES.

CARD COLUMN FORMAT ITEM EXAMPLE MEANING

24	1-2	L2	\$PLOTS	F	INDICATES PLOTS ARE NOT DESIRED.
				T	INDICATES PLOTS ARE DESIRED.
24	3-4	L2	\$MODAL	F	INDICATES PLOTS ARE FOR SUMMED SOLUTIONS ONLY.
				T	INDICATES PLOTS ARE FOR MODAL SOLUTIONS ONLY.

FOR THE REMAINDER OF CARD 24 ENTRIES, 0 INDICATES THAT NO PLOTS ARE DESIRED FOR THE PARTICULAR ITEM, AND 1 INDICATES THAT THEY ARE DESIRED. ALL GRAPHS ARE PLOTTED AS THE INDICATED ITEM VERSUS THE STATION NUMBER. IF A COMPLETE PLOT IS DESIRED, INSUTE IFREQ = 1.

CARD	COLUMN	FORMAT	ITEM	EXAMPLE	MEANING
24	5-6	I2	IRADII	1	PLCT THE RADII AS COMPUTED BY SUBROUTINE GEOM.
24	7-8	I2	IGAMMA	1	PLCT $P'/P$ AS COMPUTED BY SUBROUTINE GEOM.
24	9-10	I2	IOMEGS	1	PLCT $\omega_s$ AS COMPUTED BY SUBROUTINE GEOM.
24	11-12	I2	IOMEGT	1	PLCT $\omega_\theta$ AS COMPUTED BY SUBROUTINE GEOM.
24	13-14	I2	IDECMS	1	PLCT $\omega_s'$ AS COMPUTED BY SUBROUTINE GEOM.
24	15-16	I2	IBSTIF	1	PLCT THE STIFFNESS D AS COMPUTED BY SUBROUTINE BCB.
24	17-18	I2	IDSTIF	1	PLOT THE STIFFNESS D AS COMPUTED BY THE SUBROUTINE BCB.
24	19-20	I2	IBBSTF	1	PLCT THE STIFFNESS $db/ds$ AS COMPUTED BY SUBROUTINE BCB.
24	21-22	I2	IDDSTF	1	PLCT THE STIFFNESS $dd/ds$ AS COMPUTED BY SUBROUTINE BCB.
24	23-24	I2	IPR	1	PLOT THE NORMAL COMPONENT OF THE PRESSURE LOAD.
24	25-26	I2	IPS	1	PLOT THE MERIDIONAL COMPONENT OF THE PRESSURE LOAD.
24	27-28	I2	IPT	1	PLCT THE CIRCUMFERENTIAL COMPONENT OF THE PRESSURE LOAD.
24	29-30	I2	ITT	1	PLCT THE THERMAL LOAD.
24	31-32	I2	IMT	1	PLOT THE THERMAL MOMENT.
24	33-34	I2	IDTT	1	PLCT $d/ds$ OF THE THERMAL LOAD.
24	35-36	I2	IDMT	1	PLOT $d/ds$ OF THE THERMAL MOMENT.
24	37-38	I2	INS	1	PLOT THE MERIDIONAL MEMBRANE FORCE DISTRIBUTION.



CARD	COLUMN	FORMAT	ITEM	EXAMPLE	MEANING
24	39-40	I2	INTH	1	PLCT THE CIRCUMFERENTIAL MEMBRANE FORCE DISTRIBUTION.
24	41-42	I2	INSTH	1	PLCT THE MERIDIO-CIRCUMFERENTIAL MEMBRANE FORCE DISTRIBUTION.
24	43-44	I2	IQS	1	PLCT THE TRANSVERSE FORCE DISTRIBUTION.
24	45-46	I2	IMS	1	PLCT THE MERIDIONAL MOMENT DISTRIBUTION.
24	47-48	I2	IMTH	1	PLCT THE CIRCUMFERENTIAL MOMENT DISTRIBUTION.
24	49-50	I2	IMSTH	1	PLCT THE MERIDIO-CIRCUMFERENTIAL MOMENT DISTRIBUTION.
24	51-52	I2	IU	1	PLCT THE MERIDIONAL DISPLACEMENT DISTRIBUTION.
24	53-54	I2	IV	1	PLCT THE CIRCUMFERENTIAL DISPLACEMENT DISTRIBUTION.
24	55-56	I2	IW	1	PLCT THE NORMAL DISPLACEMENT DISTRIBUTION.
24	57-58	I2	IPHS	1	PLCT THE MERIDIONAL ROTATION DISTRIBUTION.
24	59-60	I2	IPHIT	1	PLCT THE CIRCUMFERENTIAL ROTATION DISTRIBUTION.
24	61-62	I2	IPHI	1	PLCT THE MERIDIO-CIRCUMFERENTIAL ROTATION DISTRIBUTION.

-----

INSERT IMPERFECTION DATA HERE FOR A SATANS-II OR SATANS-IIA ANALYSIS WITH IMPERFECTIONS. INSURE FORMAT OF THE IMPERFECTION DATA IS COMPATIBLE WITH THAT SPECIFIED IN THE USER-WRITTEN SUBROUTINE IMPERF.

-----

25	1-2	I2	IRNAGN	0	INDICATES THIS IS THE ONLY RUN.
				1	INDICATES ANOTHER RUN IS TO BE MADE. ACD ANOTHER COMPLETE SET OF DATA CARDS AFTER THIS CARD IS IRNAGN= 1.

APPENDIX D

LISTING OF NEW POLE ROUTINE FOR SATANS-IIA

THE FOLLOWING CARDS ARE TO BE PLACED INTO THE FORCE SUBROUTINE

CCMCMN /IBLS/IBCINL,IBCFNL

```

C   IN  FORCE
10  IF(K.NE.2.OR.(K.EQ.2.AND.IBCINL.GE.0)) GO TO 501
   DC 502  II=1,4
   SUMX=0.
   CC 503  L=1,4
   SC3  SUMX=SUMX+DL(II,L,N)*GEE(L)
   SC2  X(II,IK1)=SUMX
   SC1  CONTINUE
   CC 11  I=1,4

```

THE FOLLOWING CARDS ARE TO BE PLACED INTO THE PMATRIX SUBROUTINE

```

C   IN  PMATRIX
   CALL EFG(2,MN)
   CALL ABC
   CALL MATINV(A,4,G1,0,DETERM,IPIVCT,INDEX,4,ISCALE)
   DC 501  II=1,4
   CC 501  JJ=1,4
   CL(II,JJ,MN)=0.
   CL(II,JJ,MN)=0.
   SC1  IF(MN.GT.1) GO TO 12
   IF(MN.EQ.0) GO TO 13

```

```

MC=MN
CL(1,1,MN)=1.
CL(1,2,MN)=1.
CL(1,3,MN)=-3.
CL(1,4,MN)=-3.
CL(2,3,MN)=4.
CL(3,3,MN)=4.
CL(3,4,MN)=-1.
CL(4,4,MN)=-1.
GC TO 9C2
13
M1=MN
CL(1,1,MN)=-3.
CL(2,1,MN)=1.
CL(2,2,MN)=1.
IF(A(M1).LT.0) DL(2,2,MN)=-1
CL(3,3,MN)=1.
CL(4,4,MN)=4.
CL(4,1,MN)=-1.
GC TO 9C2
12
M2=MN
CL(1,1,MN)=1.
CL(2,2,MN)=1.
CL(3,3,MN)=1.
CL(4,4,MN)=-3.
CL(4,4,MN)=4.
CL(4,4,MN)=-1.
CCNT INUE
9C2
CC SC3 II=1,4
CC SC3 JJ=1,4
TTF=0.
L=1,4
9C4
9C5
TTF=TP+OF(I,I,L,MN)*A(L,JJ)
CL0(I,I,JJ)=TTP
CC SC5 II=1,4
CC SC5 JJ=1,4
TTF=0.
TTC=0.
9C6
9C7
TTF=TP+CL0(I,I,I,I)*C(L,JJ)
TTC=CLC(I,I,JJ)=DL(I,I,JJ,MN)-TTP
CL2(I,I,JJ)=DG(I,I,JJ,MN)-TTC
CALL MA INV(CLI,4,GI,0,DETERM,IFIVOT,INDEX,4,ISCALE)
CC SC7 II=1,4
CC SC7 JJ=1,4
TTF=0.
TTC=0.

```

```

SC8 L=114
TTP=TTQ+CL1(I,I,L)*CL0(L,JJ)
TTQ=TTQ+CL1(I,I,L)*CL2(L,JJ)
CL(I,I,JJ,MN)=-TTP
P(I,I,JJ)=TTQ
GC IC 11
SC P3=MN
SC7
SC6

```

APPENDIX E

LISTING OF CARDS FOR  $\bar{V}$  AND  $\bar{V}_{\text{MAX}}$

THE FOLLOWING CARDS ARE TO BE PLACED INTO THE DYNAMIC SUBROUTINE IF NEEDED

```

C      STATEMENTS FOR MAIN TO CALCULATE VBAR
185  DENCM=.125*GMXI(KMAX)*R(KMAX)**4
    CC 186  M=1,MAXM
    CALN=0
    MM=(M-1)*KMAX2
    CC 184  K=2,KL
    KT=K:1+MM
    184  CALN=DNLM+Z(3,KT)*R(K)
    186  CALN=DNLM*DEL#SOE
    186  VBAR(M)=DNLM/DENCM
    IF(ITTEST=ITTEST+1)
    IF(ITTEST.NE.10) GO TO 963
    ITTEST=C
    WRITE(6,183)(LSTEP,VBAR(M),M=1,MAXM))
    183  FORMAT(/5X,VBAR AT TIME STEP ',14,' FOR EACH MODE IS'/5E16.4)
    963  CC 187  M=1,MAXM
    187  IF(LSTEP.EQ.1) AVB(M)=0.
    IF(ABS(VBAR(M)).GT.AVB(M)) AVB(M)=ABS(VBAR(M))
  
```

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